Unit 5: CHEMICAL KINETICS AND EQUILIBRIA

Chapter 13: Chemical Kinetics

13.1: The Rate of a Reaction

<u>Chemical Kinetics</u>: - the branch of chemistry that studies the how fast reaction proceeds.

<u>Reaction Rates</u>: - the speed of which the concentration of a reactant or product changes per unit of time.

- unit is in $mol/(L \bullet s)$ or $mol/(L \bullet min)$

$$Rate = \frac{\Delta[A]}{\Delta t} = \frac{\text{Concentration A at } t_2 - \text{Concentration A at } t_1}{t_2 - t_1}$$

Average Rate: - like average speed, it is the change in concentration per interval of time.

Instantaneous Rate: - like instantaneous speed, it is the change in concentration at a particular time.

Example 1: The concentrations of the reactant and product of the reaction, $A \rightarrow 2 B$, are recorded below.

- a. Determine the average reaction rates for each time interval.
- b. Graph concentrations versus time for both reactant and product.
- c. Find the instantaneous reaction rates of reactant A at 20 seconds and product B at 40 seconds.

| Time (seconds) | Reactant [A] | Product [B] |
|----------------|--------------|-------------|
| 0 | 0.1 | 0 |
| 20 | 0.05 | 0.1 |
| 40 | 0.025 | 0.15 |
| 60 | 0.0125 | 0.175 |
| 80 | 0.0063 | 0.1875 |
| 100 | 0.0031 | 0.1938 |

a. Average Reaction Rates (Note: Reactant Rate is Negative because A is consumed.)

| Time Intervals (seconds) | Reactant Rate = $\frac{\Delta[A]}{\Delta t}$ (mol/(L • s) | Product Rate = $\frac{\Delta[B]}{\Delta t}$ (mol/(L • s) |
|-----------------------------|--|---|
| 0.00 to 20.00 | $\frac{(0.05 - 0.1) \text{ mol/L}}{(20.00 - 0.00) \text{ s}} = -0.002500$ | $\frac{(0.1-0) \operatorname{mol/L}}{(20.00-0.00) \operatorname{s}} = 0.005000$ |
| 20.00 to 40.00 | $\frac{(0.025 - 0.05) \text{ mol/L}}{(40.00 - 20.00) \text{ s}} = -0.001250$ | $\frac{(0.15 - 0.1) \text{ mol/L}}{(40.00 - 20.00) \text{ s}} = 0.002500$ |
| 40.00 to 60.00 | $\frac{(0.0125 - 0.025) \operatorname{mol/L}}{(60.00 - 40.00) \operatorname{s}} = -0.000625$ | $\frac{(0.175 - 0.15) \text{ mol/L}}{(60.00 - 40.00) \text{ s}} = 0.001250$ |
| 60.00 to 80.00 | $\frac{(0.0063 - 0.0125) \text{ mol/L}}{(80.00 - 60.00) \text{ s}} = -0.000310$ | $\frac{(0.1875 - 0.175) \text{ mol/L}}{(80.00 - 60.00) \text{ s}} = 0.000625$ |
| 80.00 to 100.00 | $\frac{(0.0031 - 0.0063) \text{ mol/L}}{(100.00 - 80.00) \text{ s}} = -0.000160$ | $\frac{(0.1938 - 0.1875) \text{ mol/L}}{(100.00 - 80.00) \text{ s}} = 0.000315$ |

b. Concentrations versus Time Graph.



Determining Rates Using Pressure

If a reaction starts from a solid or a liquid were to generate a gas, we can determine the rate of the reaction by measuring pressures instead of concentrations at various times. Consider the decomposition of $H_2O_{2(l)}$

$$2 H_2O_{2(l)} \rightarrow 2 H_2O_{(l)} + O_{2(g)}$$

We can measures the pressure of $O_{2(g)}$ generated to find the rate by using the Ideal Gas Law, PV = nRT.

$$P = \frac{n}{V}RT \quad \rightarrow \quad P_{\text{oxygen}} = [O_2]RT \quad \rightarrow \quad [O_2] = \frac{P_{O_2}}{RT}$$
$$Rate = \frac{\Delta[O_2]}{\Delta t} = \frac{1}{RT} \left(\frac{\Delta P_{O_2}}{\Delta t}\right)$$

<u>Rate Constant</u> (*k*): - a constant of proportionality between reaction rate and the concentration of reactant. - as the concentration of reactant increases, the reaction rate increases due to more

- chances for collisions to occur between reactants and hence the speed of the reaction increases. However, rate constant will remain the same.
 - the unit of the rate constant depends on the overall order of the reaction (explains in next section).

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 245.

For a reaction: $A \rightarrow B$ Rate = k[A]Rate = kP_Ak = rate constant $k = \frac{Rate}{[A]}$ $k = \frac{Rate}{P_A}$

(*Note: Both reaction rates are positive because they are net consumption rates.*) (The Rate Equation can follow many different form – more explanations in the next section)

Example 2: Dinitrogen pentaoxide decomposes into nitrogen dioxide and oxygen gases as follows.

 $2 \text{ N}_2\text{O}_{5(g)} \rightarrow 4 \text{ NO}_{2(g)} + \text{O}_{2(g)}$

An experiment was conducted at different initial concentrations and the rate after 1.00 minute was calculated from the final concentration as shown below. Determine the rate constant of this reaction.

| | Initial [N ₂ O ₅] | Rate (mol/L \bullet s) |
|---------|--|--------------------------|
| Trial 1 | 0.100 mol/L | 2.3×10^{-4} |
| Trial 2 | 0.050 mol/L | 1.2×10^{-4} |
| Trial 3 | 0.025 mol/L | 5.9×10^{-5} |

Trial 1:
$$k_1 = \frac{Rate_1}{[N_2O_5]_{0,1}} = \frac{2.3 \times 10^{-4} \text{ mol}/(\text{E} \cdot \text{s})}{0.100 \text{ mol}/\text{E}}$$
 $k_1 = 2.3 \times 10^{-3} \text{ s}^{-1}$
Trial 2: $k_2 = \frac{Rate_2}{[N_2O_5]_{0,2}} = \frac{1.2 \times 10^{-4} \text{ mol}/(\text{E} \cdot \text{s})}{0.050 \text{ mol}/\text{E}}$ $k_2 = 2.4 \times 10^{-3} \text{ s}^{-1}$
Trial 3: $k_1 = \frac{Rate_3}{[N_2O_5]_{0,3}} = \frac{5.9 \times 10^{-4} \text{ mol}/(\text{E} \cdot \text{s})}{0.025 \text{ mol}/\text{E}}$ $k_3 = 2.4 \times 10^{-3} \text{ s}^{-1}$

Note that the $k_1 \approx k_2 \approx k_3$. For other reactions, k would be calculated in a similar but slightly different way depending on the order of the reaction (explains in next section).

Relationship between Molar Quantities and Reaction Rates For any chemical equation, $aA + bB \rightarrow cC + dD$, $Rate = -\frac{1}{a}\frac{\Delta[A]}{\Delta t} = -\frac{1}{b}\frac{\Delta[B]}{\Delta t} = \frac{1}{c}\frac{\Delta[C]}{\Delta t} = \frac{1}{d}\frac{\Delta[D]}{\Delta t}$

Example 3: For the reaction $N_{2(g)} + 3 Cl_{2(g)} \rightarrow 2 NCl_{3(g)}$, what is the rate of consumption of N_2 and Cl_2 if the rate of production of NCl₃ is 0.453 mol/(L \bullet s)?

Rate of
$$N_2 = \frac{\Delta[N_2]}{\Delta t}$$
 $-\frac{\Delta[N_2]}{\Delta t} = -\frac{1}{3} \frac{\Delta[Cl_2]}{\Delta t} = \frac{1}{2} \frac{\Delta[NCl_3]}{\Delta t}$
Rate of $Cl_2 = \frac{\Delta[Cl_2]}{\Delta t}$ $\frac{\Delta[N_2]}{\Delta t} = -\frac{1}{2} \frac{\Delta[NCl_3]}{\Delta t} = -\frac{1}{2} (0.453 \text{ mol/(L} \cdot \text{s}))$ Rate of $N_2 = 0.227 \text{ mol/(L} \cdot \text{s})$
Rate of $NCl_3 = \frac{\Delta[NCl_3]}{\Delta t}$ $\frac{\Delta[Cl_2]}{\Delta t} = -\frac{3}{2} \frac{\Delta[NCl_3]}{\Delta t} = -\frac{3}{2} (0.453 \text{ mol/(L} \cdot \text{s}))$ Rate of $Cl_2 = 0.680 \text{ mol/(L} \cdot \text{s})$
Page 246.
Copyrighted by Gabriel Tang B.Ed., B.Sc.

13.2: The Rate Law

<u>Rate Law</u>: - a reaction rate where it is depended solely on the concentrations of the reactants with the assumption that it is an irreversible reaction.

Two Kinds of Rate Laws:

- 1. <u>Differential Rate Law</u>: sometimes called rate law, which relates the reaction rate on reactants' concentrations only.
- 2. <u>Integrated Rate Law</u>: the rate law that relates the concentration of the chemical species with time.
 it is derived by integrating the differential rate law with respect of concentration and time (explains in the next section).
- Order (*n*): the rational exponent of the reactant's concentration in the rate law as determined by experimentation. (It is <u>NOT the coefficient</u> of the chemicals.)



Overall Rate Order: - the sum of all orders of all reactants.

Example 1: For the following rate laws, determine their overall rate order and the unit of the rate constant.

a.
$$Rate = k[A]$$

 $n = 1$ (First order)
 $k = \frac{Rate}{[A]} = \frac{\text{mol}/(\pounds \circ s)}{\text{mol}/L} = s^{-1}$
b. $Rate = k[A]^2$
 $n = 2$ (Second order)
 $k = \frac{Rate}{[A]^2} = \frac{\text{mol}/(\pounds \circ s)}{(\text{mol}/L)^2} = L/(\text{mol} \circ s)$
c. $Rate = k[A][B]$
d. $Rate = k[A]^2[B]$
 $n + m = 1 + 1 = 2$
(Second order)
 $k = \frac{Rate}{[A][B]} = \frac{\text{mol}/(\pounds \circ s)}{(\text{mol}/L)^2}$
 $k = \frac{Rate}{[A][B]} = \frac{\text{mol}/(\pounds \circ s)}{(\text{mol}/L)^2}$
 $k = L/(\text{mol} \circ s)$
b. $Rate = k[A]^2$
d. $Rate = k[A]^2[B]$
 $k = \frac{Rate}{[A]^2[B]} = \frac{\text{mol}/(\pounds \circ s)}{(\text{mol}/L)^2(\text{mol}/\pounds)}$
 $k = L^2/(\text{mol}^2 \circ s)$
e. $Rate = k$
 $n = 0$ (Zero order)
 $k = \text{mol}/(L \circ s)$

Initial Rate ([A]₀): - the instantaneous reaction rate at the beginning instant (t = 0) of the reaction.

- for a single reactant, its order can be found by the instantaneous reaction rates and its concentrations at two different times.

n

Determining Rate Law of a Single Reactant using Instantaneous Rates

$$\frac{Rate \ 2}{Rate \ 1} = \frac{k[A]_{l_2}^n}{k[A]_{l_1}^n} = \left(\frac{[A]_{l_2}}{[A]_{l_1}}\right)$$

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 247.

Example 2: The decomposition of acetaldehyde (ethanal) at 298 K yields the following kinetic data.

 $CH_3CHO_{(g)} \rightarrow CH_{4(g)} + CO_{(g)}$

| Time (seconds) | [CH ₃ CHO _(g)] (mol/L) | Instantaneous Rate (mol/(L • s)) |
|----------------|---|----------------------------------|
| 0.000 | 0.400 | 1.4 |
| 0.095 | 0.300 | 0.79 |
| 0.286 | 0.200 | 0.35 |
| 0.857 | 0.100 | 0.088 |

- a. Determine the rate law and the rate constant.
- b. Graph the concentration versus time plot for the decomposition of $CH_3CHO_{(g)}$.
- c. Calculate the reaction rate when the concentration of acetaldehyde is 0.250 mol/L.
- a. To find Rate Law, pick any two concentrations and rates



 $Rate = k [CH_3 CHO]^2$ (Overall 2nd Order)

b. Concentration versus Time Graph



To calculate the Rate Constant, pick any one of the concentrations and rates.

Rate =
$$k[CH_3CHO]^2$$

 $1.4 = k(0.400 \text{ mol/L})^2$
 $\frac{1.4 \text{ mol/}(E \cdot s)}{(0.400 \text{ mol/L})^2} = k$
 $k = 8.75 \text{ L/(mol \cdot s)}$
Rate = $(8.75 \text{ L/(mol \cdot s)})[CH_3CHO]^2$

(The negative sign in k is dropped because we know reactant rate is one of consumption.)

c. When $[CH_3CHO_{(g)}] = 0.250 \text{ mol/L},$

$$Rate = (8.75 \text{ L/(mol} \cdot \text{s}))[CH_3CHO]^2$$
$$Rate = (8.75 \text{ L/(mol} \cdot \text{s}))(0.250)^2 \text{ mol}^2/\text{L}^2$$
$$Rate = 0.547 \text{ mol/(L} \cdot \text{s})$$

<u>Method of Initial Rates</u>: - the use of initial rate(s) to determine the overall rate order of the reaction.

- for x number of reactants, we will need at least (x + 1) number of experiments with various initial rates and initial concentrations.
- the order of a particular reactant is determined by dividing the initial rates of the two experiments with different initial concentrations of that particular reactant, while having the same initial concentrations of other reactants.

| Deterr | Determining Rate Law of Multiple Reactants using Initial Rates | | | |
|-----------------------------|---|--|--|--|
| $\frac{Rate \ 2}{Rate \ 1}$ | $=\frac{k[A]_{0,\exp 2}^{n}[B]_{\theta,\exp 2}^{m}}{k[A]_{0,\exp 1}^{n}[B]_{\theta,\exp 1}^{m}}=\left(\frac{[A]_{0,\exp 2}}{[A]_{0,\exp 1}}\right)^{n} \text{ where } [B]_{0,\exp 1}=[B]_{0,\exp 2}$ | | | |
| $\frac{Rate 3}{Rate 1} =$ | $= \frac{k[A]_{\theta, \exp 3}^{\mu}[B]_{0, \exp 3}^{m}}{k[A]_{\theta, \exp 4}^{\mu}[B]_{0, \exp 1}^{m}} = \left(\frac{[B]_{0, \exp 3}}{[B]_{0, \exp 1}}\right)^{m} \text{ where } [A]_{0, \exp 3} = [A]_{0, \exp 1}$ | | | |

Example 3: The formation of nitrogen dioxide from the combustion of nitrogen monoxide at 660 K gives the following kinetic data. Determine the rate law and the rate constant.

| 2 | NO | (g) + | $O_{2(g)}$ | \rightarrow | 2 | NO_2 | (g) |
|---|-----|-------|--------------|---------------|---|--------|-----|
| _ | 110 | (8) | $\sim 2 (g)$ | | _ | 1,02 | 181 |

| Experiment | [NO (g)] (mol/L) | [O _{2 (g)}] (mol/L) | Measured Initial Rate (mol/(L • s)) |
|------------|------------------|-------------------------------|-------------------------------------|
| 1 | 0.010 | 0.010 | $2.5 	imes 10^{-5}$ |
| 2 | 0.020 | 0.010 | 1.0×10^{-4} |
| 3 | 0.010 | 0.020 | $5.0 	imes 10^{-5}$ |

To find Rate Law, we first have to pick the two concentrations and rates where [O₂] stays constant.

| $\frac{Rate 2}{Rate 1} = \frac{k[NO]_{0, \exp 2}^{n}[O_{2}]_{0, \exp 2}^{m}}{k[NO]_{0, \exp 1}^{n}[O_{2}]_{0, \exp 1}^{m}}$ | $\frac{1.0 \times 10^{-4}}{2.5 \times 10^{-5}} = \frac{k(0.020 \text{ mol/L})^n (0.010 \text{ mol/L})^m}{k(0.010 \text{ mol/L})^n (0.010 \text{ mol/L})^m}$ |
|---|---|
| | $4 = (2)^n \qquad \qquad n = 2$ |
| Then, we have to pick the two concentrations and | d rates where [NO] stays constant. |
| $\frac{Rate 3}{Rate 1} = \frac{k[NO]_{0, \exp 3}^{n}[O_{2}]_{0, \exp 3}^{m}}{k[NO]^{n}[O_{2}]_{0, \exp 3}^{m}}$ | $\frac{5.0 \times 10^{-5}}{2.5 \times 10^{-5}} = \frac{k(0.010 \text{ mol/L})^{*}(0.020 \text{ mol/L})^{m}}{k(0.010 \text{ mol/L})^{m}}$ |
| $\mathbf{K}_{1}^{\mathbf{H}} \mathbf{U}_{1}^{\mathbf{H}} \mathbf{U}_{1}^{\mathbf{H}} \mathbf{U}_{1}^{\mathbf{H}} \mathbf{U}_{2}^{\mathbf{H}} \mathbf{J}_{0, \exp 1}^{\mathbf{H}} \mathbf{U}_{2}^{\mathbf{H}} \mathbf{J}_{0, \exp 1}^{\mathbf{H}}$ | $2 = (2)^m$ (0.010 mol/L) (0.010 mol/L) |
| $Rate = k[NO]^2[O_2]$ | (Overall 3 rd Order) |

To calculate the Rate Constant, we can pick the concentration and rate from any experiment.



Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 249.

Example 4: The reaction rate of the acetone iodination not only depends on the concentrations of the reactants, but it also relates to the concentration of the $H^+_{(aq)}$ ion. The rate law has a format of Rate = $k[CH_3COCH_3]^n[I_2]^m[H^+]^p$. Several experiments were done at 298 K and the initial rates of the reaction are measured. Using the data below, find the final rate law and the rate constant.

$$CH_3COCH_{3(aq)} + I_{2(aq)} \rightarrow CH_3COCH_2I_{(aq)} + H^+_{(aq)} + I^-_{(aq)}$$

| Experiment | [CH ₃ COCH _{3 (aq)}] | $\left[\mathbf{I}_{2}\left(aq\right)\right]$ | $[\mathbf{H}^{+}_{(aq)}]$ | Measured Initial Rate (mol/(L • s)) |
|------------|---|--|---------------------------|-------------------------------------|
| 1 | 0.80 mol/L | 0.001 mol/L | 0.20 mol/L | $4.2 	imes 10^{-6}$ |
| 2 | 1.6 mol/L | 0.001 mol/L | 0.20 mol/L | $8.4 	imes 10^{-6}$ |
| 3 | 0.80 mol/L | 0.001 mol/L | 0.40 mol/L | $8.4 	imes 10^{-6}$ |
| 4 | 0.80 mol/L | 0.0005 mol/L | 0.20 mol/L | $4.2 	imes 10^{-6}$ |

To find Rate Law, we first have to pick the two concentrations and rates where $[I_2]$ and $[H^+]$ stay constant.

$$\frac{Rate 2}{Rate 1} = \frac{k[CH_{3}COCH_{3}]_{0, \exp 2}^{n}[I_{2}]_{0, \exp 2}^{m}[H^{+}]_{0, \exp 2}^{p}}{k[CH_{3}COCH_{3}]_{0, \exp 1}^{n}[I_{2}]_{0, \exp 1}^{m}[H^{+}]_{0, \exp 1}^{p}} = \frac{8.4 \times 10^{-6}}{4.2 \times 10^{-6}} = \frac{k(1.6 \text{ mol/}\text{L})^{n}(\theta.\theta\theta1 \text{ mol/}\text{L})^{m}(\theta.2\theta \text{ mol/}\text{L})^{p}}{k(0.80 \text{ mol/}\text{L})^{n}(\theta.\theta\theta1 \text{ mol/}\text{L})^{m}(\theta.2\theta \text{ mol/}\text{L})^{p}}$$

$$2 = (2)^{n}$$

To find Rate Law, we first have to pick the two concentrations and rates where [CH₃COCH₃] and [H⁺] stay constant.

To find Rate Law, we first have to pick the two concentrations and rates where [I₂] and [CH₃COCH₃] stay constant.

$$\frac{Rate 3}{Rate 1} = \frac{k[CH_{3}COCH_{3}]_{0, \exp 3}^{n} [I_{2}]_{0, \exp 3}^{m} [H^{+}]_{0, \exp 3}^{p}}{k[CH_{3}COCH_{3}]_{0, \exp 1}^{n} [I_{2}]_{0, \exp 1}^{m} [H^{+}]_{0, \exp 1}^{p}} = \frac{8.4 \times 10^{-6}}{4.2 \times 10^{-6}} = \frac{k(0.80 \text{ mol/L})^{n}(0.001 \text{ mol/L})^{m}(0.40 \text{ mol/L})^{p}}{k(0.80 \text{ mol/L})^{n}(0.20 \text{ mol/L})^{p}}$$

$$2 = (2)^{p}$$

$$P = 1$$

$$Rate = k[CH_{3}COCH_{3}]^{1}[I_{2}]^{0}[H^{+}]^{1}$$

$$Rate = k[CH_{3}COCH_{3}][H^{+}]$$

$$Rate = k[CH_{3}COCH_{3}][H^{+}]$$

To calculate the Rate Constant, we can pick the concentration and rate from any experiment.

$$Rate = k[CH_{3}COCH_{3}][H^{+}]$$

$$4.2 \times 10^{-6} \text{ mol/(L} \cdot \text{s}) = k(0.80 \text{ mol/L})(0.20 \text{ mol/L})$$

$$\frac{4.2 \times 10^{-6} \text{ mol/(L} \cdot \text{s})}{(0.80 \text{ mol/L})(0.20 \text{ mol/L})} = k$$

$$Rate = (2.625 \times 10^{-5} \text{ L/(mol} \cdot \text{s}))[CH_{3}COCH_{3}][H^{+}]$$

<u>Assignment</u> 13.2 pg. 589–590 #9 to 22; pg. 593–594 #72 and 87

Page 250.

13.3: The Relationship Between Reactant Concentration and Time (Integrated Rate Law)

1. Integrated First-Order Rate Law for Single Reactant



<u>**Half-Life**</u> $(t_{\frac{1}{2}})$: - the amount of time it takes to half the original reactant's concentration.

- at half-life, $t_{\frac{1}{2}}$, the reactant's concentration is $\frac{1}{2}[\mathbf{A}]_0 = [\mathbf{A}]$: $\ln\left(\frac{[\mathbf{A}]}{[\mathbf{A}]}\right) = -kt \implies \ln\left(\frac{(\frac{1}{2}[\mathbf{A}]_{\theta})}{[\mathbf{A}]}\right) = -kt_{\frac{1}{2}} \implies \ln(\frac{1}{2}) = -kt_{\frac{1}{2}} \qquad \text{(Since } \ln(\frac{1}{2}) = -kt_{\frac{1}{2}}$

$$\frac{1}{\left[A\right]_{0}} = -kt \implies \ln\left(\frac{1}{\left[A\right]_{0}}\right) = -kt_{1/2} \implies \ln\left(\frac{1}{2}\right) = -kt_{1/2} \implies \ln\left(\frac{1}{2}\right) = -kt_{1/2} \qquad \text{(Since } \ln(\frac{1}{2}) = -\ln(2)\text{)}$$
$$\implies \ln(2) = kt_{1/2} \qquad \qquad t_{1/2} = \frac{\ln 2}{k} = \frac{0.693}{k}$$



2. Integrated Second-Order Rate Law for Single Reactant





Half-Life for Second-Order Reaction with a Single Reactant

at half-life,
$$t_{\frac{1}{2}}$$
, the reactant's concentration is $\frac{\frac{1}{2}[A]_{0}}{\left[\frac{1}{[A]}\right]} = [A]$:

$$\left(\frac{1}{[A]}\right) - \left(\frac{1}{[A]_{0}}\right) = kt \implies \left(\frac{1}{\frac{1}{2}[A]_{0}}\right) - \left(\frac{1}{[A]_{0}}\right) = kt_{\frac{1}{2}} \implies \frac{2}{[A]_{0}} - \frac{1}{[A]_{0}} = kt_{\frac{1}{2}} \implies \frac{1}{[A]_{0}} = kt_{\frac{1}{2}}$$

$$t_{\frac{1}{2}} = \frac{1}{k[A]_{0}}$$



3. Integrated Zero-Order Rate Law for Single Reactant

$$Rate = -\frac{\Delta[A]}{\Delta t} = k \qquad \text{(Starting from Zero-Order Rate Law)} \\ \Delta[A] = -k\Delta t \qquad \text{(Rearrange Equation for Integration)} \\ \int_{[A]_0}^{[A]} d[A] = -k \int_0^t dt \qquad (\Delta t = dt \text{ and } \Delta[A] = d[A]; \text{ Integrate Both Sides: } \int dx = x) \\ \textbf{[A]} - \textbf{[A]}_0 = -kt \qquad \text{(Integrated Zero Order Rate Law)} \end{cases}$$

Graphing Integrated Zero-Order Rate Law for Single Reactant



If the <u>initial graph of [A] versus t graph is a linear relation</u>, then it is a <u>Zero Order Reaction</u> with $\underline{k = -slope}$ and $\underline{[A]_0 = y\text{-intercept}}$.

Half-Life for Zero-Order Reaction with a Single Reactant

- at half-life, $t_{\frac{1}{2}}$, the reactant's concentration is $\frac{1}{2}[A]_0 = [A]$:

$$[A] - [A]_0 = -kt \implies \frac{1}{2} [A]_0 - [A]_0 = -kt_{\frac{1}{2}} \implies -\frac{[A]_0}{2} = -kt_{\frac{1}{2}} \qquad t_{\frac{1}{2}} = \frac{[A]_0}{2k}$$

Integrated Zero Order Rate Laws for Single Reactant $[A] = -kt + [A]_0$ $t_{\frac{1}{2}} = \frac{[A]_0}{2k}$ [A] = Concentration of Reactant at time t<math>k = Rate Constant $[A]_0 = Concentration of Reactant at time 0$ t = time

Example 1: The decomposition of HI $_{(g)}$ at 716 K yields the following data.

| ····(g) / / 2 ···2 (| g) + 72 + 2(g) |
|----------------------|----------------|
| Time (minutes) | [HI] mol/L |
| 0.00 | 0.02000 |
| 1.00 | 0.01248 |
| 2.00 | 0.00911 |
| 3.00 | 0.00716 |
| 4.00 | 0.00587 |
| 5.00 | 0.00501 |
| 6.00 | 0.00433 |

HI (c) $\rightarrow \frac{1}{2}$ H₂ (c) $\pm \frac{1}{2}$ I₂ (c)

- a. Complete the table below.
- b. Graph [HI] versus *t*, ln[HI] versus *t*, and 1/[HI] versus *t*. Assess the linearity to determine the overall rate order.
- c. State the integrated rate law for the decomposition of HI and find the rate constant.
- d. What is the half-life of this reaction?
- e. Calculate the time needed for the reactant to reached 10.0% of its original concentration.

| Time (minutes) | [HI] mol/L | ln[HI] | 1/[HI] |
|----------------|------------|--------|--------|
| 0.00 | 0.02000 | | |
| 1.00 | 0.01248 | | |
| 2.00 | 0.00911 | | |
| 3.00 | 0.00716 | | |
| 4.00 | 0.00587 | | |
| 5.00 | 0.00501 | | |
| 6.00 | 0.00433 | | |

- a. Using the TI-83 Plus Calculator, we can enter the experimental results in the STATS Editor and quickly manipulate the data.
- 1. Enter Values in the L₁ and L₂ Columns of Stats Editor
- Enter "ln(L₂)" in the heading of L₃.
 Enter "1/L₂" in the heading of L₄.



3. Fill in the Table

| Time (minutes) | [HI] mol/L | ln[HI] | 1/[HI] |
|----------------|------------|--------|--------|
| 0.00 | 0.02000 | -3.912 | 50 |
| 1.00 | 0.01248 | -4.384 | 80.128 |
| 2.00 | 0.00911 | -4.698 | 109.77 |
| 3.00 | 0.00716 | -4.939 | 139.66 |
| 4.00 | 0.00587 | -5.138 | 170.36 |
| 5.00 | 0.00501 | -5.296 | 199.60 |
| 6.00 | 0.00433 | -5.442 | 230.95 |

b. First, we Graph [HI] vs. t







4. Integrated Rate Law for Multiple Reactants

<u>Pseudo-First-Order Rate Law</u>: - when there are multiple reactants, if we can have excess amount for all reactants except one, we can simplify the rate law so it behaves like a first-order reaction.

Pseudo-First-Order Rate Law

For reaction with Multiple Reactants, $a\mathbf{A} + b\mathbf{B} \rightarrow \text{Products and } Rate = k[\mathbf{A}][\mathbf{B}]^n$, if $[\mathbf{B}]_0 >> [\mathbf{A}]_0$, then we can assume $[\mathbf{B}] \approx [\mathbf{B}]_0$.

We can simplify $Rate = k[A][B]^n$ to Rate = k'[A] where $k' = k[B]^n$

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 257.

- **Example 2**: A reaction, $A + 3B + 2C \rightarrow 3D + E$, has a rate law of *Rate* = $k[A][B]^2[C]$. The concentrations at the beginning of the experiment are $[A]_0 = 0.0500 \text{ mol/L}$, $[B]_0 = 2.00 \text{ mol/L}$ and $[C]_0 = 3.00 \text{ mol/L}$. After 15.0 seconds, the concentration of A is 0.0342 mol/L.
 - a. Calculate *k* for this reaction.
 - b. Determine the half-life for this reaction.
 - c. Find the concentrations of A and C after 50.0 seconds.
 - **a.** Since $[B]_0$ and $[C]_0 >> [A]_0$, we can assume that $[B] \approx [B]_0$ and $[C] \approx [C]_0$. Therefore, $Rate = k[A][B]^2[C]$ can be simplified to Rate = k'[A] where $k' = k[B]^2[C]$.

$$Rate = -k'[A]$$
(Pseudo-First-Order Rate Law)

$$ln[A] = -k't + ln[A]_{0}$$
(Pseudo-Integrated-First-Order Rate Law)

$$[A]_{0} = 0.0500 \text{ mol/L} \qquad t = 15.0 \text{ s} \qquad [A] = 0.0342 \text{ mol/L}$$

$$ln[A] - ln[A]_{0} = -k't$$

$$k' = \frac{ln[A] - ln[A]_{0}}{-t} = \frac{ln(0.0342) - ln(0.0500)}{-15.0 \text{ s}} \qquad k' = 0.0253 \text{ s}^{-1}$$

Finally, we have to convert k' back to k.

$$k' = k[\mathbf{B}]^{2}[\mathbf{C}]$$

$$k = \frac{k'}{[\mathbf{B}]^{2}[\mathbf{C}]} = \frac{(0.0253 \,\mathrm{s}^{-1})}{(2.00 \,\mathrm{mol/L})^{2}(3.00 \,\mathrm{mol/L})}$$

$$k = 0.00211 \,\mathrm{L}^{3}/(\mathrm{mol}^{3} \cdot \mathrm{s})$$

b. Because we used the Pseudo-Integrated-First-Order Rate Law, the corresponding half-life is: (*Note*: we are using k')

$$t_{1/2} = \frac{\ln(2)}{k'} = \frac{\ln(2)}{0.0253 \,\mathrm{s}^{-1}}$$
 $t_{1/2} = 27.4 \,\mathrm{s}$

c. At t = 50.0 s, [A] = ?

 $\ln[\mathbf{A}] = -\mathbf{k}'t + \ln[\mathbf{A}]_0$

Because $[C] \approx [C]_0 = 3.00 \text{ mol/L}$, at 50.0 s,

(C] ≈ 3.00 mol/L

$$\ln[A] = -(0.0253 \text{ s}^{-1})(50.0 \text{ s}) + \ln(0.0500)$$

$$\ln[A] = -4.260732274$$

$$[A] = e^{-4.260732274}$$

$$In reality, [A] reacted = [A]_0 - [A]$$

$$[A] reacted = 0.0500 \text{ mol/L} - 0.0141 \text{ mol/L}$$

$$[A] reacted = 0.0359 \text{ mol/L}$$

$$[C] reacted = \frac{2 \text{ mol C}}{1 \text{ mol A}} \times 0.0359 \text{ mol/L of A} = 0.0718 \text{ mol/L}$$

$$[C] = [C]_0 - [C] \text{ reacted} = 3.00 \text{ mol/L} - 0.0718 \text{ mol/L}$$

$$[C] = 2.93 \text{ mol/L}$$

| Order | First | Second | Zero |
|---|---|--|--|
| Rate Law | Rate = k[A] | $Rate = k[A]^2$ | Rate = k |
| Unit of <i>k</i> | s ⁻¹ or min ⁻¹ | L/(mol • s) or L/(mol • min) | $mol/(L \bullet s)$ or $mol/(L \bullet s)$ |
| Integrated Rate Law | $\ln[\mathbf{A}] = -kt + \ln[\mathbf{A}]_0$ | $\left(\frac{1}{[\mathbf{A}]}\right) = kt + \left(\frac{1}{[\mathbf{A}]_0}\right)$ | $[\mathbf{A}] = -kt + [\mathbf{A}]_0$ |
| Relationship with <i>k</i> and Linear Slope | Slope = $-k$ | Slope = k | Slope = $-k$ |
| Half-Life | $t_{\frac{1}{2}} = \frac{\ln 2}{k}$ | $t_{\frac{1}{2}} = \frac{1}{k[\mathbf{A}]_0}$ | $t_{\frac{1}{2}} = \frac{\left[\mathbf{A}\right]_{0}}{2k}$ |

Summary of Rate Laws for Reactions with Single Reactant $aA \rightarrow$ Products

Assignment 13.3 pg. 590-591 #23 to 30; pg. 594-595 #88 and 94

13.4: A Model for Chemical Kinetics

Collision Model: - a model that state for a reaction to occur, molecules must collide with each other.

Factors Affecting the Collision Model:

- 1. <u>Activation Energy</u> (E_a): the threshold energy molecules needed to overcome to cause a chemical reaction that was first proposed by Svante Arrhenius.
 - E_a is the highest energy (top of the hill E_{max}) minus the sum of energy of the reactants ($\Sigma H_{reactants}$) on the potential energy diagram.
 - Activated Complex: sometimes refer to as transition state. It is the transitional molecule found at the top "hill" of the activation energy.



Activation Energy of an Endothermic Reaction

Activation Energy of an Exothermic Reaction

2. <u>Temperature</u> (*T*): - the effective number of collisions increases exponentially with temperature.





3. <u>Molecular Orientation</u>: - the number of ways molecules collide that will lead to a reaction.





<u>Arrhenius Equation</u>: - developed by Arrehenius to relate **rate constant** (*k*) using the three factors that affect the collision model (Activation Energy, Temperature with Collision Frequency, and Steric Factor)

| $k = zp e^{\frac{-E_a}{RT}} \qquad k = A e^{\frac{-E_a}{RT}}$ | | | | | |
|---|--|------------------|---|--|--|
| k = Rate Constant z = Collision Frequency R = Gas Constant (8.314 | <i>E_a</i> = Activation <i>p</i> = Steric Facto J/(K • mol)) | Energy (J) or | <i>T</i> = Temperature (K) <i>A</i> = <i>zp</i> = Frequency Factor | | |

Linear Form of Arrhenius Equation



We can also compare the rate constants and temperature from two different points on the graph.

$$\ln(k_{2}) - \ln(k_{1}) = \left[-\frac{E_{a}}{RT_{2}} + \ln(A) \right] - \left[-\frac{E_{a}}{RT_{1}} + \ln(A) \right]$$
$$\ln(k_{2}) - \ln(k_{1}) = -\frac{E_{a}}{RT_{2}} + \frac{\ln(A)}{RT_{1}} + \frac{E_{a}}{RT_{1}} - \frac{\ln(A)}{RT_{1}} \qquad \qquad \ln\left(\frac{k_{2}}{k_{1}}\right) = \frac{E_{a}}{R} \left(\frac{1}{T_{1}} - \frac{1}{T_{2}}\right)$$

$$\frac{\text{Alternate Arrhenius Equation}}{\ln(k) = -\frac{E_a}{R} \left(\frac{1}{T}\right) + \ln(A) \qquad \ln\left(\frac{k_2}{k_1}\right) = \frac{E_a}{R} \left(\frac{1}{T_1} - \frac{1}{T_2}\right)$$

$$k = \text{Rate Constant} \qquad E_a = \text{Activation Energy (J)} \qquad T = \text{Temperature (K)}$$

$$A = \text{Frequency Factor} \qquad R = \text{Gas Constant (8.314 J/(K \bullet \text{mol}))}$$

Example 1: The decomposition of $N_2O_{4(g)} \rightarrow 2 \text{ NO}_{2(g)}$ is a first order reaction. One experiment at 274 K, its rate constant is calculated to be $4.50 \times 10^3 \text{ s}^{-1}$. At another experiment at 283 K, its rate constant was determined to be $1.00 \times 10^4 \text{ s}^{-1}$. Find the activation energy of the decomposition of $N_2O_{4(g)}$.



Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 261.

Example 2: The decomposition of $2 N_2 O_{(g)} \rightarrow 2 N_{2(g)} + O_{2(g)}$ yields the following data.

| Temperature (K) | $k (L/(mol \bullet s))$ |
|-----------------|-------------------------|
| 1125 | 11.59 |
| 1053 | 1.67 |
| 1001 | 0.38 |
| 838 | 0.0011 |

- a. Complete the table below.
- b. Graph ln(k) versus (1/T). Assess the linearity to determine the activation energy.
- c. Draw the potential energy diagram for the decomposition of N₂O_(g) at 298 K. (ΔH°_{f} = 82 kJ/mol)

| Temperature (K) | <i>k</i> (L/(mol • s) | $1/T (K^{-1})$ | $\ln(k)$ |
|-----------------|-----------------------|----------------|----------|
| 1125 | 11.5900 | | |
| 1053 | 1.6700 | | |
| 1001 | 0.3800 | | |
| 838.0 | 0.0011 | | |

- a. Using the TI-83 Plus Calculator, we can enter the experimental results in the STATS Editor and quickly manipulate the data.
 - 1. Enter Values in the L₁ and L₂ Columns of Stats Editor
- 2. Enter "1/L₁" in the heading of L₃. Enter "ln(L₂)" in the heading of L₄.



4. Fill in the Table

| Temperature (K) | $k (L/(mol \bullet s))$ | $1/T (K^{-1})$ | $\ln(k)$ |
|------------------------|-------------------------|------------------------|----------|
| 1125 | 11.5900 | 8.889×10^{-4} | 2.4501 |
| 1053 | 1.6700 | 9.497×10^{-4} | 0.5128 |
| 1001 | 0.3800 | 9.990×10^{-4} | -0.9676 |
| 838.0 | 0.0011 | 0.001193 | -6.8124 |
| | | | |



b. Graph $\ln(k)$ versus (1/T). Assess the linearity to determine the activation energy.

We can use the linear regression function of the calculator to find the value of the slope and yintercept for calculating ΔE_a and A respectively.

1. Turn Diagnostic On





c. Draw the potential energy diagram for the decomposition of N₂O (g) at 298 K. (ΔH°_{f} = 82 kJ/mol)





13.5: Reaction Mechanisms

<u>Reaction Mechanisms</u>: - the series of steps involve in most chemical reactions.

<u>Intermediates</u>: - a chemical species that is produced in the initial reaction but is consumed by the final reaction step.

- an intermediate does NOT appear in the overall reaction.

<u>Molecularity</u>: - the number of chemical species that must <u>COLLIDE</u> in a reaction step.

Elementary Step: - a reaction step for which its rate can be written based on it molecularity.

- 1. Unimolecular: an elementary step where one molecule dissociates. (A \rightarrow Products where Rate = k[A])
- 2. *Bimolecular*: an elementary step where *two* molecule collides.

 $(A + A \rightarrow \text{Products where } Rate = k[A]^2 \text{ or } A + B \rightarrow \text{Products where } Rate = k[A][B])$

3. Termolecular: - an elementary step where *three* molecule collides. $(A + A + B \rightarrow Products where Rate = k[A]^2[B] \text{ or}$

 $A + B + C \rightarrow$ Products where Rate = k[A][B][C])





Example 1: The reaction, $SO_{2(g)} + H_2O_{(l)} \rightarrow H_2SO_{3(aq)}$, has the following reaction mechanism.

 $H_{2}O_{(l)} \rightarrow H^{+}_{(aq)} + OH^{-}_{(aq)}$ $H^{+}_{(aq)} + SO_{2(g)} \rightarrow HSO_{2}^{+}_{(aq)}$ $HSO_{2}^{+} + OH^{-}_{(aq)} \rightarrow H_{2}SO_{3(aq)}$

Determine the rate law for each of the elementary step above and state their molecularity. Identify all intermediates.

| $H_2O_{(l)} \rightarrow H^+_{(aq)} + OH^{(aq)}$ $H^+_{(aq)} + SO_{2(g)} \rightarrow HSO_2^+_{(aq)}$ $HSO_2^+_{(aq)} + OH^{(aq)} \rightarrow H_2SO_{3(aq)}$ | $Rate = k_1[H_2O]$ $Rate = k_2[H^+][SO_2]$ $Rate = k_3[HSO_2^+][OH^-]$ | (Unimolecular) (Bimolecular) (Bimolecular) |
|--|--|--|
| Intermediates: H | (aq) , OH (aq) , and HSO $_{2}^{+}(aq)$ | > |

<u>Rate-Determining Step</u>: - the slowest step of the reaction mechanism for which the overall reaction rate is based on.

Deduction of Reaction Mechanism: - possible reaction mechanisms are deduced by the overall reaction rate from experimentation and chemical experience.

- a given rate law can give rise to many possible reaction mechanism. That is, a reaction mechanism can never be proven absolutely

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 265.

Two Conditions for a Possible Reaction Mechanism

- 1. All reaction steps should add up to the final balanced reaction.
- 2. The rate law as determined by experimentation must agree with the rate law of the rate-determining step.

Example 2: The reaction, $H_2O_{2(aq)} + 2 H^+_{(aq)} + 2 \Gamma_{(aq)} \rightarrow I_{2(aq)} + 2 H_2O_{(l)}$, has a experimental rate law of *Rate* = $k[H_2O_2][\Gamma^-]$. Are the following steps a possible reaction mechanism?

$$\begin{split} H_2O_2(aq) + \Gamma(aq) \rightarrow H_2O(l) + IO^{-}(aq) & (Slow) \\ H^{+}(aq) + IO^{-}(aq) \rightarrow HIO(aq) & (Fast) \\ HIO(aq) + H^{+}(aq) + \Gamma^{-}(aq) \rightarrow I_2(aq) + H_2O(l) & (Fast) \\ \end{split}$$

$$\begin{split} H_2O_2(aq) + I^{-}(aq) \rightarrow H_2O(l) + IO^{-}(aq) & (Slow) \\ H^{+}(aq) + IO^{-}(aq) \rightarrow H_2O(l) + IO^{-}(aq) & (Fast) \\ \hline H^{+}(aq) + IO^{-}(aq) \rightarrow HO^{-}(aq) & (Fast) & Rate-determining step: \\ Rate = k_1[H_2O_2][I^{-}] \\ \hline HIO^{-}(aq) + I^{+}(aq) + I^{-}(aq) \rightarrow I_2(aq) + H_2O(l) & (Fast) \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & (Fast) \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 I^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 H^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & Rate = k[H_2O_2][I^{-}] \\ \hline H_2O_2(aq) + 2 H^{+}(aq) + 2 H^{-}(aq) \rightarrow I_2(aq) + 2 H_2O(l) & H^{-}(aq) & H^$$

Steps of the Reaction Mechanism added up to the final reaction (1st condition met). Rate-determining elementary step gives the same rate law compared to that from experiments (2nd condition met). Therefore, the proposed mechanism is a possible pathway for the overall final reaction.

13.6: Catalysis

<u>Catalyst</u>: - a substance that speeds up the reaction <u>without</u> being consumed in the reaction.

- unlike intermediates, catalyst is used and recycled in the reaction.
- lowers activation energy by providing an alternate reaction pathway. $(\Delta E_a \text{ is lowered but } \Delta H_{rxn} \text{ remains the same.})$



Three Types of Catalyst

- 1. <u>Heterogeneous Catalyst</u>: a catalyst that exists in a different phase compared to the reactants.
 - utilizes the concept of **adsorption** to **"hold down"** the reactants for faster reaction rate.

Adsorption: - collection of a substance on the surface of another substance.

- the opposite of *absorption* (passing a substance through another).

In general, heterogeneous catalytic reaction involves four steps.

- 1. Adsorption of the reactants and activation of the heterogeneous catalyst on the surface.
- 2. *Migration* of the adsorbed reactants on the catalytic surface.
- 3. *Reaction* of the adsorbed substances.
- 4. *Desorption* or release of the products.

Examples: a. Ammonia is formed from its elements using heterogeneous catalyst such as Pt_(s):

$$N_{2(g)} + 3 H_{2(g)} \xrightarrow{Pt} 2 NH_{3(g)}$$

(Check out Video at http://www.dac.neu.edu/physics/b.maheswaran/phy1121/data/ch11/anim/anim11-5b.mov)



b. The catalytic converter converts NO $_{(g)}$ (result of burning nitrogen at high temperature) to N_{2 (g)} and O_{2 (g)}. The O_{2 (g)} along with the catalytic converter is used to produce CO_{2 (g)} from CO $_{(g)}$.

A catalytic converter for most modern vehicle. Leaded gasoline deactivates catalytic converter. Therefore, they are not legally used in vehicles

- 2. <u>Homogeneous Catalyst</u>: a catalyst that exists in the same phase as the reactants.
- **Example 1**: The destruction of ozone in upper atmosphere can be attributed to $NO_{(g)}$ and CFCs acting as catalysts. $NO_{(g)}$ is produced from the combustion of $N_{2(g)}$ at high temperature commonly found in internal combustion engine (high-altitude aircraft produces lots of $NO_{(g)}$). CFCs (chloro-fluoro-carbon compounds) are found in aerosol can propellants, refrigerators, and air conditioners. They break down to form $Cl_{(g)}$ with the presence of light. Use the following two reaction mechanisms; identify the intermediates and catalysts for the decomposition processes of ozone in the upper atmosphere.

$$\begin{array}{c} \operatorname{NO}_{(g)} + \operatorname{O}_{3}_{(g)} \rightarrow \operatorname{NO}_{2}_{(g)} + \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + \operatorname{NO}_{2}_{(g)} \rightarrow \operatorname{NO}_{(g)} + O_{2}_{(g)} \\ \overline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + \operatorname{O}_{3}_{(g)} \rightarrow \operatorname{ClO}_{(g)} + \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + \operatorname{ClO}_{3}_{(g)} \rightarrow \operatorname{Cl}_{(g)} + O_{2}_{(g)} \\ \overline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow \operatorname{ClO}_{(g)} + O_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow \operatorname{ClO}_{(g)} + O_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow \operatorname{ClO}_{(g)} + O_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow \operatorname{ClO}_{(g)} + O_{2}_{(g)} \\ \underline{O}_{(g)} + \operatorname{ClO}_{(g)} \rightarrow \operatorname{Cl}_{(g)} + O_{2}_{(g)} \\ \underline{O}_{(g)} + \operatorname{ClO}_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow \operatorname{ClO}_{(g)} + O_{2}_{(g)} \\ \underline{O}_{(g)} + \operatorname{ClO}_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + \operatorname{ClO}_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow \operatorname{Cl}_{(g)} + O_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \\ \underline{O}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array} \qquad \begin{array}{c} \operatorname{Cl}_{(g)} + O_{3}_{(g)} \rightarrow 2 \operatorname{O}_{2}_{(g)} \end{array}$$

How Ozone is Destroyed



TOMS Ozone Sep 10, 2000 - Min: 125 DU; ~Area: 29.2×106 km2



(Above) The Ozone Hole over the South Pole (Sept 2000). A similar hole is present over the Arctic. (Left) Process of Ozone Depletion. Ozone blocks harmful UV rays that can otherwise cause skin cancer.

- 3. <u>Enzyme Catalyst</u>: a biological catalysts that speeds up certain types of chemical reaction in living beings. an enzyme is typically a large protein molecule.
 - an average cell can consist of over 3000 different enzymes.
 - a specific enzyme only acts on specific molecule called substrate (or reactant). It can be viewed as the "lock-and-key" model as first developed by Emil Fischer in 1894 (see diagram below).
 - many enzymes have multiple active sites for the interactions of substrates.
 - thermodynamically, the main goal of enzymes is to lower ΔG , thereby increasing thermodynamic spontaneity. ΔS is reduced by bringing the substrates in the correct orientation to react.
 - kinetically, the speed of the reaction is increased due to lowering of the energy of the activation complex (transition state). Some enzymes can catalyze the forward and reverse reaction equally, such as carbonic anhydrase. In either case, the activation energy is lowered.



Chapter 14: Chemical Equilibrium

14.1: The Concept of Equilibrium and the Equilibrium Constant

<u>Chemical Equilibrium</u>: - the state at which the concentrations of all reactants and products remain

- constant with time (<u>the Forward Reaction Rate = Reverse Reaction Rate</u>).
 <u>the equilibrium state is dynamic (not static)</u>. Chemical species are continuously converting from reactants to products and vice versa. It appears that the reaction has stopped only because the rate of consumption = rate of production.
- if an equilibrium state is disturbed (changing concentrations of species, pressure, volume and temperature change), the reaction will shift towards one side in order to re-establish the new equilibrium state.
- like reaction rate, **Equilibrium is affected by Temperature**.



(Check out Video at http://www.mhhe.com/physsci/chemistry/animations/chang_7e_esp/kim2s2_5.swf)



<u>The N₂O_{4 (g)} \Rightarrow 2 NO_{2 (g)} equilibrium</u>.

Initially (Picture A), there were very little $NO_{2(g)}$. As time proceeded forward, more $NO_{2(g)}$ (brown color) is produced (Pictures B & C). However, there are still $N_2O_{4(g)}$ present at the equilibrium state (Picture D).

Law of Mass Action: - a reversible reaction at equilibrium and a constant temperature, a certain ratio of reactant and product concentrations (**Equilibrium Expression**) has a constant value, *K* – **equilibrium constant**.

Equilibrium Expression: - an expression <u>relating the concentrations or pressures of the reactants and</u> products when they are at the state of equilibrium.

- it takes the form of the individual products raised to the power of their respective coefficients divided by the individual reactants raised to the power of their respective coefficients.
- the equilibrium expression is <u>unique</u> for each reaction, but <u>it is the same</u> <u>for that particular reaction regardless of temperature</u>.

Equilibrium Constant (K): - the <u>unitless</u> numerical value of the equilibrium expression.

- the equilibrium constant is the same for a particular reaction if it remains at the same temperature.

Equilibrium Expression and Constant of a Reaction $aA + bB \Rightarrow cC + dD$ $K = \frac{[C]^k [D]^d}{[A]^a [B]^b} \leftarrow Equilibrium Expressions$ a and b: Coefficients of reactant species A and B c and d: Coefficients of product species C and D [A], [B], [C] & [D] = Equilibrium Concentrations of Chemicals K = Equilibrium Constant (Concentrations)

> <u>Assignment</u> 14.1 pg. 633 #1 to 4

14.2: Writing Equilibrium Constant Expressions

Homogeneous Equilibria: - an equilibrium system where all chemical species are in the same phase.

- **Equilibrium Constant** (*K*): the symbol for equilibrium constant when the expression deals with **concentrations** is simply *K* or K_c . When the expression deals with pressures, it is symbolized as K_P .
 - for equilibrium of an ideal system, the activity of a substance is the ratio of its concentration or partial pressure to a standard value of 1 M or 1 atm. The procedure eliminates all units but does not alter the numerical value of the concentrations and pressures. Therefore, *K* has no units.



Example 1: Write the equilibrium expression of the following reactions.



<u>Equilibrium Position</u>: - the concentrations or pressures of all chemical species at equilibrium state.
 <u>depends strongly on the Initial Concentrations of the chemical species</u>. (In contrast, *K* does <u>NOT</u> depend on initial concentrations, only on temperature and the specific reaction.)

- since there all many possible initial concentrations for any one reaction, <u>there are infinite number of</u> equilibrium position for a particular reaction.
- *Note*: Do NOT confuse initial concentrations [A]₀ with equilibrium concentration [A]_{eq}!! We only use Equilibrium Concentrations to calculate K by substituting them into the equilibrium expression.
- **Example 2**: The formation of HI_(g) is an equilibrium reaction. Several experiments are performed at 710 K using different initial concentrations.

| Experi | Iment I | Experiment 2 | | | |
|--|--|------------------------------------|--|--|--|
| Initial | Equilibrium | Initial | Equilibrium | | |
| $[H_2]_0 = 0.100 M$ | $[H_2]_{eq} = 0.0222 \text{ M}$ | $[H_2]_0 = 0 M$ | $[H_2]_{eq} = 0.0350 \text{ M}$ | | |
| $[I_2]_0 = 0.100 \text{ M}$ | $[I_2]_{eq} = 0.0222 \text{ M}$ | $[I_2]_0 = 0.0100 \text{ M}$ | $[I_2]_{eq} = 0.0450 \text{ M}$ | | |
| $[HI]_0 = 0 M$ | $[HI]_{eq} = 0.156 \text{ M}$ | $[HI]_0 = 0.350 \text{ M}$ | $[HI]_{eq} = 0.280 \text{ M}$ | | |
| Experi | iment 3 | Experiment 4 | | | |
| Initial | Equilibrium | Initial | Equilibrium | | |
| | | | | | |
| $[H_2]_0 = 0.00150 \text{ M}$ | $[H_2]_{eq} = 0.0150 \text{ M}$ | $[H_2]_0 = 0 M$ | $[H_2]_{eq} = 0.0442 \text{ M}$ | | |
| $[H_2]_0 = 0.00150 \text{ M}$ $[I_2]_0 = 0 \text{ M}$ | $[H_2]_{eq} = 0.0150 \text{ M}$ $[I_2]_{eq} = 0.0135 \text{ M}$ | $[H_2]_0 = 0 M$ $[I_2]_0 = 0 M$ | $[H_2]_{eq} = 0.0442 \text{ M}$ $[I_2]_{eq} = 0.0442 \text{ M}$ | | |

$$H_{2(g)} + I_{2(g)} \rightleftharpoons 2 HI_{(g)}$$

a. Write the equilibrium expression for the formation of $HI_{(g)}$.

b. Calculate the equilibrium constant for each experiment, and average them for an overall value.



Converting K_c to K_P:

$$PV = nRT$$
(Ideal Gas Law) $P = \left(\frac{n}{V}\right)RT = CRT$ (Solving for P and let $\frac{n}{V} = Concentration)$ $K_P = \frac{P_C^c P_D^d}{P_A^a P_B^b}$ (Equilibrium Expression and Constant for $aA + bB \Rightarrow cC + dD$)

Substituting pressures for each chemical species into the equilibrium expression: $(P_A = [A]RT; P_B = [B]RT; P_C = [C]RT; and P_D = [D]RT)$

$$K_{P} = \frac{\left(\left[C\right]RT\right)^{c}\left(\left[D\right]RT\right)^{d}}{\left(\left[A\right]RT\right)^{a}\left(\left[B\right]RT\right)^{b}} = \frac{\left[C\right]^{c}\left(RT\right)^{c}\left[D\right]^{d}\left(RT\right)^{d}}{\left[A\right]^{a}\left(RT\right)^{a}\left[B\right]^{b}\left(RT\right)^{b}}$$

$$K_{P} = \frac{\left[C\right]^{c}\left[D\right]^{d}\left(RT\right)^{c+d}}{\left[A\right]^{a}\left[B\right]^{b}\left(RT\right)^{a+b}} = \frac{\left[C\right]^{c}\left[D\right]^{d}}{\left[A\right]^{a}\left[B\right]^{b}}\left(RT\right)^{(c+d)-(a+b)}$$

$$K_{P} = K_{c}(RT)^{(c+d)-(a+b)}$$
(Combine exponents on common base RT using Laws of Exponents)
(Replace $\frac{\left[C\right]^{c}\left[D\right]^{d}}{\left[A\right]^{a}\left[B\right]^{b}}$ with K_{c})

 $\frac{\text{Conversion between Concentration and Pressure Equilibrium Constants}}{aA + bB \rightleftharpoons cC + dD}$ $K_P = K_c (RT)^{\Delta n}$ where $\Delta n = \Sigma$ Coefficients of Products $-\Sigma$ Coefficients of Reactants = (c + d) - (a + b) $R = 0.08206 \text{ K}^{-1}$ T = Temperature in K R has a unit of K^{-1} to cancel out with the Kelvin from Temperature only, therefore K calculated will remain unitless **Example 3**: One possible way of removing NO $_{(g)}$ from the exhaust of an internal combustion engine is to cause it to react with CO $_{(g)}$ in the presence of suitable catalyst.

$$2 \text{ NO}_{(g)} + 2 \text{ CO}_{(g)} \rightleftharpoons N_{2(g)} + 2 \text{ CO}_{2(g)}$$

At 575 K, the reaction has $K = 2.2 \times 10^{59}$. What is K_P of the same reaction at 575 K?

 $K = K_c = 2.2 \times 10^{59} \qquad K_P = K_c (RT)^{\Delta n} \\ R = 0.08206 \text{ K}^{-1} \qquad K_P = (2.2 \times 10^{59})[(0.08206 \text{ K}^{-1})(575 \text{ K})]^{-1} \\ T = 575 \text{ K} \qquad K_P = (2.2 \times 10^{59})[47.1845]^{-1} \\ \Delta n = \Sigma n_{\text{products}} - \Sigma n_{\text{reactants}} \\ \Delta n = (1+2) - (2+2) = 3 - 4 \\ \Delta n = -1 \\ K_P = ?$

Example 4: The German's Haber-Bosch process developed in 1913 utilizes an iron surface that contains traces of aluminium and potassium oxide as a catalyst to manufacture ammonia from nitrogen and hydrogen. It is an important process as ammonia is commonly used in fertilizer and ammunition. In 1918, the scientist Fritz Haber won the Nobel Prize in chemistry for his contribution.

$$N_{2(g)} + 3 H_{2(g)} \rightleftharpoons 2 NH_{3(g)}$$

- a. At 400 K, $P_{\text{NH}_3} = 0.1024$ atm, $P_{\text{N}_2} = 2.8084$ atm and $P_{\text{H}_2} = 0.0102$ atm. Write the equilibrium expression in terms of pressure and calculate K_P .
- b. Convert the calculated K_P above to K.

a. Equilibrium Expression:
$$K_P = \frac{P_{NH_3}^2}{P_{N_2}P_{H_2}^3}$$
 Equilibrium Constant: $K_P = \frac{(0.1024)^2}{(2.8084)(0.0102)^3}$
b. $K_P = 3.52 \times 10^3$
 $R = 0.08206 \text{ K}^{-1}$ $T = 400 \text{ K}$ $K_P = K_c (RT)^{\Delta n}$
 $\Delta n = \sum n_{\text{products}} - \sum n_{\text{reactants}}$ $K_c = \frac{K_P}{(RT)^{\Delta n}} = \frac{(3.52 \times 10^3)}{[(0.08206 \text{ K}^{-1})(400 \text{ K})]^{-2}}$ $K_c = 3.79 \times 10^7$
 $\Delta n = -2$
 $K_P = ?$

Heterogeneous Equilibria: - an equilibrium system where some chemical species are in different phase compare to the others.

- <u>chemical species that are Pure Solid or Pure Liquid are NOT Included in</u> <u>the Equilibrium Expression</u>. This is due to the fact that pure solids and liquids do not have concentrations.

Unit 5: Chemical Kinetics and Equilibria

Example 5: Write the equilibrium expression for the following systems.

a. $2 \operatorname{NaN}_{3(s)} \rightleftharpoons 2 \operatorname{Na}_{(s)} + 3 \operatorname{N}_{2(g)}$



c. $\operatorname{Ag_2SO_4}_{(s)} \rightleftharpoons 2\operatorname{Ag}^+_{(aq)} + \operatorname{SO_4}^{2-}_{(aq)}$

 $K = [Ag^+]^2 [SO_4^{2^-}]$ (Ag₂SO₄ is a Pure Solid) (No K_P because there are no gases.)



(No K_P because there are no gases.)

<u>Multiple Equilibria</u>: - the overall equilibrium constant of a multi-steps systems is the <u>product</u> of all the equilibrium constants of the individual steps involved.

Consider the following multiple equilibria:



Working with Equilibrium Constant and Equations:

reversing equilibrium reaction will cause the reciprocate the equilibrium constant (1/K)
multiplying the equation by a multiple *n* will result in raising the K by the power of *n*.

| Reversing Equilibrium Reaction | Multiplying Equilibrium Reaction by a Factor of <i>n</i> |
|--|--|
| $a\mathbf{A} + b\mathbf{B} \rightleftharpoons c\mathbf{C} + d\mathbf{D} \rightarrow c\mathbf{C} + d\mathbf{D} \rightleftharpoons a\mathbf{A} + b\mathbf{B}$ | $n(a\mathbf{A} + b\mathbf{B} \rightleftharpoons c\mathbf{C} + d\mathbf{D}) \rightarrow na\mathbf{A} + nb\mathbf{B} \rightleftharpoons nc\mathbf{C} + nd\mathbf{D})$ |
| $K' = \frac{[A]^{a}[B]^{b}}{[C]^{c}[D]^{d}} = \left(\frac{[C]^{c}[D]^{d}}{[A]^{a}[B]^{b}}\right)^{-1} = K^{-1} = \frac{1}{K}$ $K' = \text{Reverse Equilibrium Constant}$ | $K^{"} = \frac{\left[\mathbf{C}\right]^{nc} \left[\mathbf{D}\right]^{nd}}{\left[\mathbf{A}\right]^{na} \left[\mathbf{B}\right]^{nb}} = \left(\frac{\left[\mathbf{C}\right]^{k} \left[\mathbf{D}\right]^{d}}{\left[\mathbf{A}\right]^{a} \left[\mathbf{B}\right]^{b}}\right)^{n} = K^{n}$ $K^{"} = \text{New Equilibrium Constant}$ |

Example 6: For the following reaction and the equilibrium concentrations at 300 K.

$$2 C_{3}H_{6(g)} + 2 NH_{3(g)} + 3 O_{2(g)} \approx 2 C_{3}H_{3}N_{(g)} + 6 H_{2}O_{(g)}$$

$$[C_{3}H_{6}]_{eq} = 0.500 M [NH_{3}]_{eq} = 0.250 M [O_{2}]_{eq} = 0.350 M$$

$$[C_{3}H_{3}N]_{eq} = 2.50 M [H_{2}O]_{eq} = 3.00 M$$

- a. Write the equilibrium expression and determine the equilibrium constant.
- b. Write the equilibrium expression and calculate the equilibrium constant for the following reaction with the same equilibrium concentrations.

$$2 C_{3}H_{3}N_{(g)} + 6 H_{2}O_{(g)} \Rightarrow 2 C_{3}H_{6(g)} + 2 NH_{3(g)} + 3 O_{2(g)}$$

c. Write the equilibrium expression and find the equilibrium constant for the following reaction with the same equilibrium concentrations.



<u>Assignment</u> 14.2 pg. 633–635 #5 to 11, 13, 14, 16, 18, 20, 22 to 24, 26 to 28, 30 to 32; pg. 639 #92

14.3: The Relationship Between Chemical Kinetics and Chemical Equilibrium

Suppose we have the following elementary steps of an overall system, $aA + bB \Rightarrow cC + dD$

| Step 1: | $a\mathbf{A} + b\mathbf{B} \rightleftharpoons n\mathbf{A}\mathbf{B}$ | (at a specific <i>T</i> , the forward rate = reverse rate) $k_{f,1}[\mathbf{A}]^{a}[\mathbf{B}]^{b} = k_{r,1}[\mathbf{AB}]^{n}$ |
|----------|--|--|
| Step 2: | $nAB \Rightarrow cC + dD$ | (at the same specific <i>T</i> , the forward rate = reverse rate) $k_{f,2}[AB]^n = k_{r,2}[C]^c[D]^d$ |
| Overall: | $a\mathbf{A} + b\mathbf{B} \rightleftharpoons c\mathbf{C} + d\mathbf{D}$ | |

Equilibrium Constant (K) can be written as the ratio of rate constants of the forward and reverse reactions.

For Step 1, we have $K_1 = \frac{k_{f,1}}{k_{r,1}} = \frac{[AB]^n}{[A]^a [B]^b}$. Similarly, for Step 2, we have $K_2 = \frac{k_{f,2}}{k_{r,2}} = \frac{[C]^c [D]^d}{[AB]^n}$.

From what we have learned about multiple equilibria (section 14.2), $K = K_1 \times K_2$. Therefore,

$$K = \frac{k_{f,1}}{k_{r,1}} \times \frac{k_{f,2}}{k_{r,2}} \qquad \longrightarrow \qquad K = \frac{\left[\mathbf{AB}\right]^n}{\left[\mathbf{A}\right]^a \left[\mathbf{B}\right]^b} \times \frac{\left[\mathbf{C}\right]^c \left[\mathbf{D}\right]^d}{\left[\mathbf{AB}\right]^n}$$

Now, the overall reaction of, $a\mathbf{A} + b\mathbf{B} \Rightarrow c\mathbf{C} + d\mathbf{D}$, would have an equilibrium expression of $\mathbf{K} = \frac{[\mathbf{C}]^{k}[\mathbf{D}]^{d}}{[\mathbf{A}]^{k}[\mathbf{B}]^{k}}$.

Since the rate constant is dependent on temperature, and equilibrium constant is a ratio of rate constants,

Equilibrium Constant (K) is highly dependent on temperature (T).

<u>Assignment</u> 14.3 pg. 635 #33 and 34

14.4: What Does the Equilibrium Constant Tell Us?

Important Notes Regarding the Size of the Equilibrium Constant (K):

$$a\mathbf{A} + b\mathbf{B} \rightleftharpoons c\mathbf{C} + d\mathbf{D}$$
$$K = K_c = \frac{\left[\mathbf{C}\right]_{eq}^c \left[\mathbf{D}\right]_{eq}^d}{\left[\mathbf{A}\right]_{eq}^a \left[\mathbf{B}\right]_{eq}^b} \qquad K_P = \frac{P_{\mathbf{C},eq}^c P_{\mathbf{D},eq}^d}{P_{\mathbf{A},eq}^a P_{\mathbf{B},eq}^b}$$

- 1. When K >> 1, the equilibrium system favours the products. There are more products than reactants at the state of equilibrium. ([C]_{eq} and [D]_{eq} or $P_{C, eq}$ and $P_{D, eq} >> [A]_{eq}$ and [B]_{eq} or $P_{A, eq}$ and $P_{B, eq}$)
- 2. When $\underline{K \leq 1}$, the equilibrium system favours the reactants. There are less products than reactants at the state of equilibrium. ([A]_{eq} and [B]_{eq} or $P_{A, eq}$ and $P_{B, eq} >> [C]_{eq}$ and $[D]_{eq}$ or $P_{C, eq}$ and $P_{D, eq}$)
- 3. When $\underline{K \approx 1}$, the equilibrium system <u>favours neither the products nor the reactants</u>. <u>There are</u> <u>roughly the same amount of products and reactants at the state of equilibrium</u>. ([C]_{eq} and [D]_{eq} or $P_{C, eq}$ and $P_{D, eq} \approx [A]_{eq}$ and $[B]_{eq}$ or $P_{A, eq}$ and $P_{B, eq}$)
- 4. The <u>Size of K has NO Relationship with the Rate of Reaction</u> to reach the state of equilibrium. <u>Reaction Rate is dependent on Activation Energy</u> and <u>Temperature (T)</u> (NOT K).
- 5. The Size of K depends on Free Energy (G) and Temperature (T).

<u>Reaction Quotient</u> (*Q*): - the mass action expression under any set of conditions (not necessarily equilibrium).

- its magnitude relative to K determines the direction in which the reaction must occur to establish equilibrium.

$$\boldsymbol{Q} = \frac{\left[\mathbf{C}\right]^{c} \left[\mathbf{D}\right]^{d}}{\left[\mathbf{A}\right]^{a} \left[\mathbf{B}\right]^{b}}$$

- a. When Q > K, the system shifts to the reactants. At a specific condition, <u>Q indicates that there are too</u> <u>much products</u>. Therefore, the system has to shift back to the left.
- b. When *Q* < *K*, the system shifts to the products. At a specific condition, *Q indicates that there are* <u>not enough products</u>. Therefore, the system has to shift forward to the right.
- c. <u>When Q = K, the system is at equilibrium</u>. At a specific condition, <u>*Q* indicates that all</u> <u>concentrations are that of the equilibrium state</u>. Therefore, there will be no shifting.

Example 1: The reaction, $2 \operatorname{NO}_{(g)} + \operatorname{O}_{2(g)} \rightleftharpoons 2 \operatorname{NO}_{2(g)}$ has an equilibrium constant of K = 29.54 at 600 K. Indicate the direction in which the system will shift to reach equilibrium when the $[\operatorname{NO}]_0 = 0.300 \text{ M}, [\operatorname{O}_2]_0 = 0.250 \text{ M}$, and $[\operatorname{NO}_2]_0 = 0.500 \text{ M}$.

| $[NO]_0 = 0.300 \text{ M}$ $[O_2]_0 = 0.250 \text{ M}$ $[NO_2]_0 = 0.500 \text{ M}$ | $Q = \frac{\left[NO_{2}\right]_{0}^{2}}{\left[NO\right]_{0}^{2}\left[O_{2}\right]_{0}} = \frac{\left(0.500\right)^{2}}{\left(0.300\right)^{2}\left(0.250\right)}$ |
|---|---|
| <i>Q</i> = ? | Since $Q \le K$ (11.1 < 29.54), <u>the system will shift to the product</u> (NO ₂). There are not enough NO ₂ at the initial conditions. |

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 277.

Example 2: The reaction, $Cl_{2(g)} + 3 F_{2(g)} \rightleftharpoons 2 ClF_{3(g)}$ at 350 K has K = 50.2, If the equilibrium concentrations of $Cl_{2(g)}$ and $ClF_{3(g)}$ are 0.149 M and 0.205 M respectively, what is the equilibrium concentration of $F_{2(g)}$?

| $[Cl_2]_{eq} = 0.149 \text{ M}$ $[ClF_3]_{eq} = 0.205 \text{ M}$ K = 50.2 | $K = \frac{\left[\operatorname{ClF}_3\right]_{eq}^2}{\left[\operatorname{Cl}_2\right]_{eq}\left[\operatorname{F}_2\right]_{eq}^3}$ | $50.2 = \frac{(0.205)^2}{(0.149)[F_2]_{eq}^3}$ | |
|---|--|---|--------------------------------|
| $[F_2]_{eq} = ?$ | | $[\mathbf{F}_2]^{3}_{eq} = \frac{(0.205)^2}{(50.2)(0.149)}$ | |
| | | $[\mathbf{F}_2]_{eq} = \sqrt[3]{\frac{(0.205)^2}{(50.2)(0.149)}}$ | $[F_2]_{eq} = 0.178 \text{ M}$ |

- <u>ICE Box</u>: stands for <u>Initial, Change, and Equilibrium</u>. It is a table that organizes information to calculate final equilibrium concentrations given the equilibrium constant and initial concentration.
- **Example 3**: The formation of HCl_(g) from its elements, H_{2 (g)} + Cl_{2 (g)} \rightleftharpoons 2 HCl_(g) has K = 0.404 at 250 K. A 5.00 L flask at 250 K contained an initial concentration of 3.00 mol of HCl_(g) and 3.85 mol of H_{2 (g)}. When the system reached equilibrium, it was found that there were 0.860 mol of Cl_{2 (g)}. Determine the concentrations of H_{2 (g)} and HCl_(g) at equilibrium.

$$K = 0.404$$

$$[H_2]_0 = \frac{3.85 \text{ mol}}{5.00 \text{ L}} = 0.770 \text{ M}$$

$$[HC1]_0 = \frac{3.00 \text{ mol}}{5.00 \text{ L}} = 0.600 \text{ M}$$

$$[Cl_2]_0 = 0 \text{ M}$$

$$[Cl_2]_{eq} = \frac{0.860 \text{ mol}}{5.00 \text{ L}} = 0.172 \text{ M}$$

The system must shift to the left because initially, we are missing one reactant ($[Cl_2]_0 = 0$ M). Hence, the change to the H₂ is positive, and the change to the HCl would be negative.

Since there is 0.172 M of Cl₂ at equilibrium, it means 0.172 M of H₂ is added (1:1 mol ratio between Cl₂ and H₂). It also means that there is 2(0.172 M) less HCl (2:1 mol ratio between Cl₂ and HCl).

| $[H_2]_{eq} = ?$ | | $\mathbf{H}_{2(g)}$ | + | $\operatorname{Cl}_{2(g)}$ | # | 2 HCl (g) |
|---------------------------|-------------|---------------------|---|----------------------------|---|-------------|
| $[\mathbf{HCl}]_{eq} = ?$ | Initial | 0.770 M | | 0 M | | 0.600 M |
| | Change | + 0.172 M | | + 0.172 M | | -2(0.172 M) |
| | Fauilibrium | 0 942 M | | 0 172 M | | 0 256 M |

Verify with *K*:

$$K = \frac{[\text{HCl}]_{eq}^2}{[\text{H}_2]_{eq}[\text{Cl}_2]_{eq}} = \frac{(0.256)^2}{(0.942)(0.172)}$$

This matches with *K* given in the question.

Therefore, the equilibrium concentrations are:

 $[H_2]_{eq} = 0.942 \text{ M}, [Cl_2]_{eq} = 0.172 \text{ M} \text{ and } [HCl]_{eq} = 0.256 \text{ M}$

Page 278.

Example 4: The reaction, $2 \text{ NO}_{2(g)} \rightleftharpoons \text{NO}_{3(g)} + \text{NO}_{(g)}$ has K = 31.7 at 700 K. A 2.50 L flask at 700 K has 1.00 mol of each species initially. Calculate the concentrations of all species at equilibrium.

$$K = 31.7$$

[NO₂]₀ = $\frac{1.00 \text{ mol}}{2.50 \text{ L}} = 0.400 \text{ M}$
[NO₃]₀ = $\frac{1.00 \text{ mol}}{2.50 \text{ L}} = 0.400 \text{ M}$
[NO]₀ = $\frac{1.00 \text{ mol}}{2.50 \text{ L}} = 0.400 \text{ M}$

 $[NO_2]_{eq} = ?$ $[NO_3]_{eq} = ?$ $[NO]_{eq} = ?$ First, we must determine Q and the direction of the shift.

$$Q = \frac{[\text{NO}_3]_0[\text{NO}]_0}{[\text{NO}_2]_0^2} = \frac{(0.400)(0.400)}{(0.400)^2} \qquad Q = 1.00$$

Since $Q \le K$ (1.00 < 31.7), <u>the system will shift to the products</u> (NO₃ and NO). There are not enough products at the initial conditions. Hence, the change to the NO₂ is negative, and the changes to the NO₃ and NO would be positive.

Let x = amount of change per mole, since there are 2 moles of NO₂ reacted; NO₂ will be lowered by 2x. Similarly, NO₃ and NO will be increased by 1x each.

| | 2 NO _{2 (g)} | # | NO _{3 (g)} | + | NO (g) |
|-------------|-----------------------|---|---------------------|---|---------------|
| Initial | 0.400 M | | 0.400 M | | 0.400 M |
| Change | -2x | | +x | | +x |
| Equilibrium | (0.400 - 2x) M | | (0.400 + x) M | | (0.400 + x) M |

Next, we set up the equilibrium expression, substitute the above mathematical expressions and solve for *x*.

(Since we have a set of common exponents we can group it and square root both sides.)

$$K = \frac{[\text{NO}_3]_{eq}[\text{NO}]_{eq}}{[\text{NO}_2]_{eq}^2} \qquad 31.7 = \frac{(0.4+x)(0.4+x)}{(0.4-2x)^2} = \frac{(0.4+x)^2}{(0.4-2x)^2} = \left[\frac{(0.4+x)}{(0.4-2x)}\right]^2$$

$$\sqrt{31.7} = \sqrt{\left[\frac{(0.4+x)}{(0.4-2x)}\right]^2}$$

$$5.630275304 = \frac{(0.4+x)}{(0.4-2x)}$$

$$5.630275304 (0.4-2x) = 0.4+x$$

$$2.252110122 - 11.26055061x = 0.4+x$$

$$-12.26055061x = -1.852110122$$

$$x = \frac{-1.852110122}{-12.26055061}$$

$$x = 0.15106$$

$$\text{NO}_2]_{eq} = 0.400 + 100 +$$

Verify with K: $K = \frac{[NO_3]_{eq}[NO]_{eq}}{[NO_2]_{eq}^2} = \frac{(0.551)(0.551)}{(0.0979)^2} \qquad K = 31.7$ This metabols with the K given in the question

This matches with the *K* given in the question.

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Finally, substitute x back into the mathematical expressions.

$$[NO_{2}]_{eq} = 0.400 - 2x = 0.400 - 2(0.15106)$$
$$[NO_{2}]_{eq} = 0.400 + x = 0.400 + (0.15106)$$
$$[NO_{3}]_{eq} = 0.400 + x = 0.400 + (0.15106)$$
$$[NO]_{eq} = 0.400 + x = 0.400 + (0.15106)$$
$$[NO]_{eq} = 0.551 M$$

Page 279.

<u>Using the TI-Graphing Calculator to Solve Higher Degree Equations</u>:

Sometimes we may encounter equations with higher degrees when solving for equilibrium pressures or concentrations. In some cases, we may be able to use the quadratic formula, but for cubic and higher degrees equations, they can become quite difficult. The TI-Graphing Calculator has a SOLVE function to aide the determination of the roots.

Example: Solve for the final concentrations of both products in the following equilibrium system when the initial concentration of the reactant is 0.400 mol/L, and $K = 2.4 \times 10^{-2}$.

| $\mathbf{A}_{(g)} \rightleftharpoons \mathbf{B}_{(g)} + \mathbf{C}_{(g)}$ | | | | | | |
|---|---------------|---|--------------------|---|------------|--|
| | A (g) | # | $\mathbf{B}_{(g)}$ | + | C (g) | |
| Initial | 0.400 M | | 0 M | | 0 M | |
| Change | - <i>x</i> | | +x | | +x | |
| Equilibrium | (0.400 - x) M | | <i>x</i> M | | <i>x</i> M | |



Therefore, the concentrations of the products are:

$$x = [B]_{eq} = [C]_{eq} = 0.0867 \text{ mol/L}$$

Example 5: The reaction, $SO_{2(g)} + Cl_{2(g)} \Rightarrow SO_2Cl_{2(g)}$, has an equilibrium constant of 0.486 at 500 K. Determine the equilibrium concentrations of all species if there are 2.00 mol of each species in 10.0 L container at 500 K.

| K = 0.486 |] |
|--|---|
| $[SO_2]_0 = \frac{2.00 \text{ mol}}{10.0 \text{ L}} = 0.200 \text{ M}$ | |
| $[Cl_2]_0 = \frac{2.00 \text{ mol}}{10.0 \text{ L}} = 0.200 \text{ M}$ | |
| $[\mathrm{SO}_2\mathrm{Cl}_2]_0 = \frac{2.00 \text{ mol}}{10.0 \text{ L}} = 0.200 \text{ M}$ | 1 |

 $[SO_2]_{eq} = ?$ $[Cl_2]_{eq} = ?$ $[SO_2Cl_2]_{eq} = ?$ First, we must determine Q and the direction of the shift. $Q = \frac{[SO_2Cl_2]_0}{[SO_2]_0[Cl_2]_0} = \frac{(0.200)}{(0.200)(0.200)} \qquad Q = 5.00$

Since $Q \ge K$ (5.00 > 0.486), *the system will shift to the reactants* (SO₂ and Cl₂). There is too much product at the initial conditions. Hence, the changes to the SO₂ and Cl₂ are positive, and the change to the SO₂Cl₂ would be negative.

Let x = amount of change per mole, since there is 1 mole of SO₂ reacted; SO₂ will increase by 1x. Similarly, Cl₂ will increase by 1x. SO₂Cl₂, on the other hand, will decrease by 1x.

| | SO _{2 (g)} | + | $\operatorname{Cl}_{2(g)}$ | # | $SO_2Cl_{2(g)}$ |
|-------------|---------------------|---|----------------------------|---|-----------------|
| Initial | 0.200 M | | 0.200 M | | 0.200 M |
| Change | +x | | +x | | -x |
| Equilibrium | (0.200 + x) M | | (0.200 + x) M | | (0.200 - x) M |

Next, we set up the equilibrium expression, substitute the above mathematical expressions and solve for *x*.

(Since we don't have any common exponent, we have to expand the denominator.)

$$K = \frac{\left[SO_{2}Cl_{2}\right]_{eq}}{\left[SO_{2}\right]_{eq}\left[Cl_{2}\right]_{eq}} \qquad 0.486 = \frac{(0.2 - x)}{(0.2 + x)(0.2 + x)} = \frac{(0.2 - x)}{(0.04 + 0.4x + x^{2})} \\ 0.486 (0.04 + 0.4x + x^{2}) = (0.2 - x) \\ 0.01944 + 0.1944x + 0.486x^{2} = 0.2 - x \\ 0.486x^{2} + 1.1944x - 0.18056 = 0 \qquad (Quadratic Equation: Apply the Quadratic Formula!) \\ x = \frac{-b \pm \sqrt{b^{2} - 4ac}}{2a} \qquad a = 0.486 \qquad b = 1.1944 \qquad c = -0.18056 \\ x = \frac{-(1.1944) \pm \sqrt{(1.1944)^{2} - 4(0.486)(-0.18056)}}{2(0.486)} \qquad Finally, substitute x back into the mathematical expressions. \\ \left[SO_{2}\right]_{eq} = 0.200 + x = 0.200 + (0.14287) \\ x = 0.14287 \qquad x = -2.6005 \text{ (omit negative x)} \end{cases}$$

Verify with K:

$$K = \frac{\left[\text{SO}_2\text{Cl}_2\right]_{eq}}{\left[\text{SO}_2\right]_{eq}\left[\text{Cl}_2\right]_{eq}} = \frac{(0.0571)}{(0.343)(0.343)} \qquad K = 0.485$$

This matches closely with the *K* given in the question.

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 281.

 $[Cl_2]_{eq} = 0.200 + x = 0.200 + (0.14287)$

 $[Cl_2]_{eq} = 0.343 \text{ M}$

 $[SO_2Cl_2]_{eq} = 0.200 - x = 0.200 - (0.14287)$

 $[SO_2Cl_2]_{eq} = 0.0571 \text{ M}$

Steps to Solve Equilibrium Problems:

- 1. <u>Write the Balanced Chemical Equation for the system.</u> This <u>includes all the correct states</u> for all species.
- 2. Write the <u>Equilibrium Expression</u> and equate it to K value given.
- 3. List the Initial Concentrations.
- 4. <u>Determine *Q* and compare it to *K* to determine the direction of the shift to equilibrium.</u>
- 5. Construct the ICE Box and define the change amount of change per mole as x. Using the
- coefficients and the direction of the shifts, state the mathematical expressions of each species at equilibrium.
- 6. Solve for x after substituting the mathematical expressions into the equilibrium expression. (Look for methods of simplifying like common exponents if they exist. Otherwise, the quadratic equation will be needed to solve for x.)
- 7. <u>Calculate the equilibrium concentrations</u> of each species and <u>verify that they indeed give the value</u> <u>of *K*.</u>
- 8. For equilibrium involving pressures, the procedure is the same as above.
- **Example 6**: The equilibrium constant for the system, $C_2H_{6(g)} + Cl_{2(g)} \rightleftharpoons C_2H_5Cl_{(s)} + HCl_{(g)}$, at 283 K is 0.100. If we had 6.00 mol of $C_2H_{6(g)}$, 6.00 mol of $Cl_{2(g)}$ and 6.00 mol HCl_(g) originally in a 3.00 L container at 283 K, determine the equilibrium concentrations for all species.

$$K = 0.100$$

$$[C_{2}H_{6}]_{0} = \frac{6.00 \text{ mol}}{3.00 \text{ L}} = 2.00 \text{ M}$$

$$[Cl_{2}]_{0} = \frac{6.00 \text{ mol}}{3.00 \text{ L}} = 2.00 \text{ M}$$

$$[HCl]_{0} = \frac{6.00 \text{ mol}}{3.00 \text{ L}} = 2.00 \text{ M}$$

$$[C_{2}H_{6}]_{eg} = ?$$

 $[C_2 H_6]_{eq} = ?$ $[Cl_2]_{eq} = ?$ $[HCl]_{eq} = ?$ First, we must determine *Q* and the direction of the shift. (Be careful! This is a heterogeneous system. C₂H₅Cl is a pure solid and it is not involved in the equilibrium expression.

$$Q = \frac{[\text{HCl}]_0}{[\text{C}_2\text{H}_6]_0[\text{Cl}_2]_0} = \frac{(2.00)}{(2.00)(2.00)} \qquad \qquad Q = 0.500$$

Since Q > K (0.500 > 0.100), <u>the system will shift to the reactants</u> (C₃H₆ and Cl₂). There are too much products at the initial conditions. Hence, the changes to the C₂H₆ and Cl₂ are positive, and the change to the HCl would be negative.

Let x = amount of change per mole, since there is 1 mole of C₂H₆ reacted; C₂H₆ will increase by 1x. Similarly, Cl₂ will increase by 1x. HCl, on the other hand, will decrease by 1x.

| | $C_2H_{6(g)}$ | + | $\operatorname{Cl}_{2(g)}$ | # | $C_2H_5Cl_{(s)}$ | + | HCl _(g) |
|-------------|---------------|---|----------------------------|---|------------------|---|--------------------|
| Initial | 2.00 M | | 2.00 M | | | | 2.00 M |
| Change | +x | | +x | | | | -x |
| Equilibrium | (2.00 + x) M | | (2.00 + x) M | | | | (2.00 - x) M |

Next, we set up the equilibrium expression, substitute the above mathematical expressions and solve for *x*.

(Since we have a set of common exponents we can group it and square root both sides.)

$$K = \frac{[\text{HCI}]_{0}}{[\text{C}_{2}\text{H}_{6}]_{0}[\text{Cl}_{2}]_{0}} \qquad 0.100 = \frac{(2-x)}{(2+x)(2+x)} = \frac{(2-x)}{(4+4x+x^{2})}$$

$$0.100 (4 + 4x + x^{2}) = (2-x)$$

$$0.4 + 0.4x + 0.1x^{2} = 2-x$$

$$0.1x^{2} + 1.4x - 1.6 = 0$$

$$x = \frac{-b \pm \sqrt{b^{2} - 4ac}}{2a} \qquad a = 0.1 \qquad b = 1.4 \qquad c = -1.6$$

$$x = \frac{-(1.4) \pm \sqrt{(1.4)^{2} - 4(0.1)(-1.6)}}{2(0.1)} \qquad \text{Finally, substitute x back into the mathematical expressions.}$$

$$x = 1.062258 \quad x = -15.06226 \text{ (omit negative x)} \qquad [\text{C}_{2}\text{H}_{6}]_{eq} = 2.00 + x = 2.00 + (1.062257748)$$

$$(\text{Cl}_{2}]_{eq} = 3.06 \text{ M}$$

$$(\text{Cl}_{2}]_{eq} = 3.06 \text{ M}$$

$$(\text{Cl}_{2}]_{eq} = 3.06 \text{ M}$$

$$(\text{HCI}]_{eq} = 0.0 - x = 2.00 - (1.062257748)$$

$$(\text{HCI}]_{eq} = 0.038 \text{ M}$$

Example 7: The reaction of $CO_{(g)} + Cl_{2(g)} \rightleftharpoons COCl_{2(g)}$ has an equilibrium constant of $K_P = 0.289$ at 450 K. The initial pressures of $CO_{(g)}$, $Cl_{2(g)}$ and $COCl_{2(g)}$ are 0.800 atm, 0.900 atm and 0.150 atm respectively. They are all mixed in a 7.50 L flask at 450 K. Find the equilibrium pressures.

 $K_P = 0.289$ $P_{CO, 0} = 0.800$ atm $P_{Cl_{2,0}} = 0.900$ atm $P_{COCl_{2,0}} = 0.150$ atm First, we must determine *Q* and the direction of the shift.

$$Q_P = \frac{P_{\text{COCl}_2,0}}{P_{\text{CO},0}P_{\text{Cl}_2,0}} = \frac{(0.150)}{(0.800)(0.900)} \qquad Q_P = 0.208$$

 $P_{\text{CO}, eq} = ?$ $P_{\text{CI}_2, eq} = ?$ $P_{\text{COCI}_2, eq} = ?$

Since $Q \le K$ (0.208 < 0.289), <u>the system will shift to the product</u> (COCl₂). There is too little product at the initial conditions. Hence, the changes to the CO and Cl₂ are negative, and the change to the COCl₂ would be positive.

Let x = amount of change per mole, since there is 1 mole of CO reacted; CO will decrease by 1x. Similarly, Cl₂ will decrease by 1x. COCl₂, on the other hand, will increase by 1x.

| | CO (g) | + | $\operatorname{Cl}_{2(g)}$ | # | $\operatorname{COCl}_{2(g)}$ |
|-------------|-----------------|---|----------------------------|---|------------------------------|
| Initial | 0.800 atm | | 0.900 atm | | 0.150 atm |
| Change | -x | | -x | | +x |
| Equilibrium | (0.800 - x) atm | | (0.900 - x) atm | | (0.150 + x) M |



Next, we set up the equilibrium expression, substitute the above mathematical expressions and

14.5: Factors That Affect Chemical Equilibrium

Le Châtelier's Principle: - a qualitative method to predict the shift on an equilibrium system if it is disturbed by means of <u>changing concentration</u>, pressure and temperature.
- the equilibrium will shift in the direction that minimizes the change imposed on the system.

- 1. Effects of a Change in Concentration:
 - a. <u>An ADDITION of a species on one side of the equilibrium will Drive the System TOWARDS the</u> <u>Opposite Side.</u> (There is more concentration of the species being added. Hence, the system will <u>shift</u> towards the opposite side to reduce the increased amount of that particular species.)
 - b. <u>A REMOVAL of a species on one side of the equilibrium will Drive the system TOWARDS the Same Side.</u> (There is less concentration of the species being removed. Hence, the system will shift towards the removal side to compensate.)



Changes in Concentrations on Equilibrium System $aA + bB \Rightarrow cC + dD$

Time

- ① <u>indicates an Increase in [D]</u>. As [D][↑], equilibrium shifts to the left ($aA + bB \Rightarrow cC + dD$). Hence, [A][↑], [B][↑], and [C]↓.
- ② <u>indicates a Decrease in [A]</u>. As [A]↓, equilibrium shifts to the left $(aA + bB \neq cC + dD)$. Hence, [B]↑, [C]↓, and [D]↓.
- ③ <u>indicates an Increase in [B]</u>. As [B][↑], equilibrium shifts to the right $(aA + bB \Rightarrow cC + dD)$. Hence, [A] \downarrow , [C][↑], and [D][↑].
- ④ <u>indicates a Decrease in [C]</u>. As [C]↓, equilibrium shifts to the right $(aA + bB \Rightarrow cC + dD)$. Hence, [A]↓, [B]↓, and [D]↑.

2. Effects of a Change in Pressure:

- **a.** <u>Adding an Inert Gas has NO CHANGE on the equilibrium system</u>. This is because an inert gas does not participate in the forward or reverse reaction.
- b. <u>Reducing the Volume will Drive the System TOWARDS the Side With LESS Gaseous Molecules</u>. Since there are less space for the number of molecules, the system will have to shift to the side with lesser gaseous molecules to compensate.
- c. Conversely, <u>Expanding the Volume will Drive the System TOWARDS the Side With MORE</u> <u>Gaseous Molecules</u>. Now that there is more room for the molecules to move about, the system will shift to the side that has more gaseous molecules to adjust to the new condition.
- d. <u>When there are Equal Number of Gaseous Molecules on Both Side of the Equilibrium, any</u> <u>Change in Volume will NOT Affect System.</u>

Changes in Pressures on a Gaseous Equilibrium System $aA + bB \Rightarrow cC + dD$ when (c + d) > (a + b)



① <u>indicates an Increase in Volume</u>. As V[↑], equilibrium shifts to the right $(aA + bB \Rightarrow cC + dD)$ since there are more gaseous molecules on the product side [(c + d) > (a + b)]. Hence, $[A] \downarrow$, $[B] \downarrow$, $[C] \uparrow$, and $[D] \uparrow$.

- ② <u>indicates a Decrease in Volume</u>. As V↓, equilibrium shifts to the left $(aA + bB \Rightarrow cC + dD)$ since there are LESS gaseous molecules on the reactant side [(c + d) > (a + b)]. Hence, $[A]^{\uparrow}$, $[B]^{\uparrow}$, $[C]\downarrow$, and $[D]\downarrow$.
- 3 <u>indicates an Addition of an Inert Gas</u>. There is no shifting of the equilibrium. $(aA + bB \Rightarrow cC + dD)$ as inert gas does not affect the system. Hence, [A], [B], [C], and [D] remain unchanged.

(See the Video at http://www.sasked.gov.sk.ca/docs/chemistry/mission2mars/contents/chapter3/images/pn2o4.mpg)

- 3. Effects of a Change in Temperature: *look at the energy (written in the reactant or product side) as* <u>*a chemical species.*</u> Then, the predictions will be the same as those found with changing the concentrations.
 - a. For an <u>Exothermic Equilibrium System</u>: $aA + bB \Rightarrow cC + dD + Energy$
 - an <u>Increase in Temperature</u> will drive the system to the left ($aA + bB \Rightarrow cC + dD + Energy$). There is more heat added and because energy is written on the product side, the system will shift to the opposite side to re-establish equilibrium. Hence, $[A]\uparrow$, $[B]\uparrow$, $[C]\downarrow$, and $[D]\downarrow$.
 - a <u>Decrease in Temperature</u> will drive the system to the right ($aA + bB \Rightarrow cC + dD + Energy$). There is less heat overall and because energy is written on the product side, the system will shift to the products to compensate. Hence, $[A]\downarrow$, $[B]\downarrow$, $[C]\uparrow$, and $[D]\uparrow$.

- **b.** For <u>Endothermic Equilibrium System</u>: $aA + bB + Energy \Rightarrow cC + dD$
 - a <u>Decrease in Temperature</u> will drive the system to the left $(aA + bB + Energy \Rightarrow cC + dD)$. There is less heat overall and because energy is written on the reactant side, the system will shift to the reactants to compensate. Hence, $[A]\uparrow$, $[B]\uparrow$, $[C]\downarrow$, and $[D]\downarrow$.
 - an <u>Increase in Temperature</u> will drive the system to the right $(aA + bB + Energy \Rightarrow cC + dD)$. There is more heat added and because energy is written on the reactant side, the system will shift to the opposite side to re-establish equilibrium. Hence, $[A]\downarrow$, $[B]\downarrow$, $[C]\uparrow$, and $[D]\uparrow$.



- ① <u>indicates a Decrease in Temperature</u>. As $T \downarrow$, equilibrium shifts to the right of an exothermic system ($aA + bB \Rightarrow cC + dD + Energy$). Hence, $[A] \downarrow$, $[B] \downarrow$, $[C] \uparrow$, and $[D] \uparrow$.
- ② <u>indicates an Increase in Temperature</u>. As T^\uparrow , equilibrium shifts to the left of an exothermic system ($aA + bB \Rightarrow cC + dD + Energy$). Hence, [A]↑, [B]↑, [C]↓, and [D]↓.
- ③ <u>indicates an Increase in Temperature</u>. As T^{\uparrow} , equilibrium shifts to the right of an endothermic reaction $(aA + bB + Energy \Rightarrow cC + dD)$. Hence, $[A] \downarrow$, $[B] \downarrow$, $[C]^{\uparrow}$, and $[D]^{\uparrow}$.
- ④ <u>indicates a Decrease in Temperature</u>. As $T \downarrow$, equilibrium shifts to the left of an endothermic reaction ($aA + bB + Energy \Rightarrow cC + dD$). Hence, $[A]\uparrow$, $[B]\uparrow$, $[C]\downarrow$, and $[D]\downarrow$.
- 4. <u>Effects of Adding a Catalyst</u>: <u>has NO CHANGE on the equilibrium system.</u> (See Video at <u>http://www.sasked.gov.sk.ca/docs/chemistry/mission2mars/contents/chapter3/images/catalyst.avi</u>)

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 287.

- **Example 1**: The equilibrium system, $4 PF_{3(g)} \Rightarrow P_{4(s)} + 6 F_{2(g)} + 1578 kJ$, is put under the following changes. Predict the shift of the system and the resulting concentrations of all species for each case.
- a. an increase in the concentration of $F_{2(g)}$.

The system will shift to the LEFT. $4 \operatorname{PF}_{3(g)} \rightleftharpoons \operatorname{P}_{4(s)} + 6 \operatorname{F}_{2(g)} \uparrow + 1578 \text{ kJ}$

```
Effect: [PF<sub>3</sub>]<sup>↑</sup> (increase)
```

c. a decrease in the concentration of $PF_{3(g)}$.

The system will shift to the LEFT. 4 $\mathbf{PF_{3(g)}} \downarrow \Rightarrow \mathbf{P}_{4(s)} + 6 \mathbf{F}_{2(g)} + 1578 \text{ kJ}$

Effect: [F₂]↓ (decrease)

e. an addition of $\operatorname{He}_{(g)}$.

There will be NO SHIFT on the system.

 $4 \text{ PF}_{3(g)} \rightleftharpoons P_{4(s)} + 6 \text{ F}_{2(g)} + 1578 \text{ kJ}$

(He is an inert gas and does not involve with the equilibrium system)

Effect: [PF₃] and [F₂] remain the same.

b. a decrease in the concentration of $P_{4(s)}$

There will be NO SHIFT on the system.

 $4 \operatorname{PF}_{3(g)} \rightleftharpoons \operatorname{P}_{4(s)} \downarrow + 6 \operatorname{F}_{2(g)} + 1578 \text{ kJ}$

(P₄ is a pure solid and does not involve with the equilibrium system)

Effect: [PF₃] and [F₂] remain the same.

d. a decrease in Temperature.

The system will shift to the RIGHT.

$$4 \text{ PF}_{3(g)} \Rightarrow P_{4(s)} + 6 \text{ F}_{2(g)} + 1578 \text{ kJ} \downarrow$$

Effect: $[PF_3]\downarrow$ (decrease) and $[F_2]\uparrow$ (increase)

f. an increase in volume.

The system will shift to the RIGHT.

4 $PF_{3(g)} \Rightarrow P_{4(s)} + 6 F_{2(g)} + 1578 kJ$

(There are more gaseous molecules on the product side -6 moles of $F_{2(g)}$ versus 4 moles of $PF_{3(g)}$)

Effect: $[PF_3] \downarrow$ (decrease) and $[F_2] \uparrow$ (increase)

Example 2: The Haber-Bosch process, $N_{2(g)} + 3 H_{2(g)} \rightleftharpoons 2 NH_{3(g)} + 92 kJ$ is essentially an equilibrium system. A chemical engineer would like the highest yield of ammonia. List all the possible method of production that will ensure maximum amount of $NH_{3(g)}$ produced.

 $N_{2(g)} + 3 H_{2(g)} \Rightarrow 2 NH_{3(g)} + 92 kJ$ (Desire Effect: $[NH_3]\uparrow$, which means driving the system forward.)

- 1. <u>Increase the concentrations of $N_{2(g)}$ or $H_{2(g)}$ or both will drive the system forward.</u>
- 2. Decrease the concentration of $NH_{3(g)}$ as it is produced will shift the system forward.
- 3. <u>Lower the Temperature</u> will drive the system to the product side.
- 4. <u>Decrease the Volume of the system</u> will shift the system to the right due to smaller number of gaseous molecules on the product side.

Assignment

14.5 pg. 636–640 #49 to 52, 56 to 62 (even), 65 to 69, 90, 98, 106

18.6: Free Energy and Chemical Equilibrium

<u>Relationship between Free Energy and Pressure</u>: - the free energy of a gas at any pressure, G, can be calculated when comparing it to the free energy at standard pressures (1 atm), G° , along with the stated temperature in Kelvin and the gas constant.

| Deletionship between Free | Enorgy on | Drossuro |
|---|--|---|
| $G = G^{\circ} + RT$ | $\frac{1}{\Gamma \ln(P)}$ | |
| G = Free Energy (J) of the gas <u>at Pressure of P at</u> G° = Free Energy (J) of gas <u>at Standard Pressure</u> | <u>m</u> of 1 atm | R = Gas Constant 8.314 J/K T = Temperature in K P = Pressure of Gas in atm |
| When $P = 1$ atm, then $G = G^{\circ} + RT$ ln | (1) and <i>G</i> = | G° because $\ln(1) = 0$ |
| Calculating the ΔG of a System with Gaseous Product | s and React | tants at any Pressure, <u>P</u> : |
| $a\mathbf{A}_{(g)} + b\mathbf{B}_{(g)} \rightleftharpoons c$ | $C_{(g)} + dD_{(g)}$ | |
| $\Delta G = cG_{\rm C} + dG_{\rm D} - aG_{\rm A} - bG_{\rm B}$ | $(\Delta G =$ | $\Sigma nG_{\text{products}} - \Sigma nG_{\text{reactants}})$ |
| $\Delta G = c[G^{\circ}_{\mathrm{C}} + RT \ln(P_{\mathrm{C}})] + d[G^{\circ}_{\mathrm{D}} + RT \ln(P_{\mathrm{D}})] - a[G^{\circ}_{\mathrm{A}} + RT \ln(P_{\mathrm{D}})] - a[G^{\circ}_$ | $+ \frac{RT}{RT} \ln(P_A)$] (Expan | $-b[G^{\circ}_{B} + RT \ln(P_{B})]$ and each term using $G = G^{\circ} + RT \ln(P)$ |
| $\Delta G = cG^{\circ}_{\mathrm{C}} + cRT \ln(P_{\mathrm{C}}) + dG^{\circ}_{\mathrm{D}} + dRT \ln(P_{\mathrm{D}}) - aG^{\circ}_{\mathrm{A}} - dC^{\circ}_{\mathrm{A}}$ | $aRT \ln(P_A) - (Multi)$ | $-bG^{\circ}_{B} - bRT \ln(P_{B})$ ply moles into each brackets) |
| $\Delta G = [c \ G^{\circ}_{\mathrm{C}} + dG^{\circ}_{\mathrm{D}} - aG^{\circ}_{\mathrm{A}} - bG^{\circ}_{\mathrm{B}}] + cRT \ln(P_{\mathrm{C}}) + dRT$ (Col | $\ln(P_{\rm D}) - aR$ lect G° term | $\frac{dT \ln(P_{\rm A}) - bRT \ln(P_{\rm B})}{dG^{\circ}_{\rm D} - aG^{\circ}_{\rm A} - bG^{\circ}_{\rm B}]} = \Delta G^{\circ}$ |
| $\Delta G = \Delta G^{\circ} + \frac{RT}{c} \ln(P_{\rm C}) + \frac{d}{d} \ln(P_{\rm D}) - \frac{a}{d} \ln(P_{\rm A}) - \frac{b}{d} \ln(P_{\rm B})$ |)] (Take o | out common factor <i>RT</i> from other terms |
| $\Delta G = \Delta G^{\circ} + \frac{RT}{RT} \left[\ln(P_{\rm C}^{\ c}) + \ln(P_{\rm D}^{\ d}) - \ln(P_{\rm A}^{\ a}) - \ln(P_{\rm B}^{\ b}) \right]$ | (Apply | law of logarithm: $n \log x = \log x^n$) |
| $\Delta G = \Delta G^{\circ} + RT \ln \left(\frac{P_{\rm C}^{c} P_{\rm D}^{d}}{P_{\rm A}^{a} P_{\rm B}^{b}} \right) \qquad \text{[Apply logarithm laws: 1]}$ | ogm + logn | $= \log(mn)$ and $\log m - \log n = \log(m/n)$] |
| $\Delta G = \Delta G^{\circ} + \mathbf{RT} \ln (\mathbf{Q})$ | [Subst | itute Reaction Q as $\left(\frac{P_{\rm C}^{c}P_{\rm D}^{d}}{P_{\rm A}^{a}P_{\rm B}^{b}}\right)$] |
| Free Energy and Pressures of Gaseou | s System <mark>a</mark> A | $(a) + bB_{(g)} \rightleftharpoons cC_{(g)} + dD_{(g)}$ |
| $\Delta G = \Delta G^{\circ}$ | $+ RT \ln(Q)$ | |

 $\Delta G = \text{Free Energy (J) of the gas <u>at Pressure of P atm</u>}$ $<math display="block">\Delta G^{\circ} = \text{Free Energy (J) of gas <u>at Standard Pressure of 1 atm</u>}$ $Q = \text{Reaction Quotient of Gaseous Species} = \left(\frac{P_{\text{C}}^{c} P_{\text{D}}^{d}}{P_{\text{A}}^{a} P_{\text{B}}^{b}}\right)$ R = Gas Constant 8.314 J/KT = Temperature in K

When Q = 1, then $\Delta G = \Delta G^{\circ} + RT \ln(1)$ and $\Delta G = \Delta G^{\circ}$ because $\ln(1) = 0$

Example 1: At 25°C, the system, 2 NO $_{(g)}$ + Cl_{2 $(g) \approx$} 2 NOCl $_{(g)}$ has the following partial pressures of NO $_{(g)}$, Cl_{2 (g)}, and NOCl $_{(g)}$ are 2.40 atm, 5.30 atm and 3.25 atm respectively. Determine the change in free energy for the system at the partial pressures indicated. (*G*° of NO $_{(g)}$ = 87 kJ/mol, *G*° of Cl_{2 (g)} = 0 kJ/mol and*G* $° of NOCl <math>_{(g)}$ = 66 kJ/mol)</sub>

| $G^{\circ}_{NO} = 87 \text{ kJ/mol}$ | $2 \operatorname{NO}_{(g)} + \operatorname{Cl}_{2(g)} \rightleftharpoons 2 \operatorname{NOCl}_{(g)}$ |
|---|--|
| $G^{\circ}_{Cl_2} = 0 \text{ kJ/mol}$ | $\Delta G^{\circ} = \Sigma G^{\circ}_{\text{products}} - \Sigma G^{\circ}_{\text{reactants}}$ |
| $G^{\circ}_{\text{NOCl}} = 66 \text{ kJ/mol}$ | $\Delta G^{\circ} = [(2 \text{ mol})(66 \text{ kJ/mol})] - [(2 \text{ mol})(87 \text{ kJ/mol}) + (1 \text{ mol})(0 \text{ kJ/mol})]$ |
| $P_{\rm NO} = 2.40 {\rm atm}$ | $\Delta G^{\circ} = -42 \text{ kJ} = -4.2 \times 10^4 \text{ J} (\Delta G^{\circ} < 0; \text{ Forward Reaction is Spontaneous})$ |
| $P_{Cl_2} = 5.30 \text{ atm}$ | P^2_{NOCL} (3.25) ² |
| $P_{\rm NOCl} = 3.25$ atm | $Q = \frac{100 Q_2}{P^2_{\text{NO}} P_{\text{Cl}_2}} = \frac{1}{(2.40)^2 (5.30)} \qquad Q = 0.3459938417$ |
| $T = 25^{\circ}\text{C} = 298.15 \text{ K}$ | $\Delta G = \Delta G^{\circ} + RT \ln(Q)$ |
| $\Delta G^{\circ} = ? Q = ?$ | $\Delta G = (-4.2 \times 10^4 \text{ J}) + (8.314 \text{ J/K})(298.15 \text{ K}) \ln(0.3459938417)$ |
| $\Delta G = ?$ | $\Delta G = -44630.85574 \text{ J}$ |
| | $\Delta G = -45 \text{ kJ}$ |
| | (It became more spontaneous towards the product side. This probably means that $Q < K$ or $K > 0.346$) |

Example 2: At 25°C, the system, $H_2O_{(g)} + Cl_2O_{(g)} \Rightarrow 2 \operatorname{HOCl}_{(g)}$ has the following partial pressures of $H_2O_{(g)}$, $Cl_2O_{(g)}$, and $\operatorname{HOCl}_{(g)}$ are 0.350 atm, 0.220 atm and 0.860 atm respectively. Determine the change in free energy for the system at the partial pressures indicated. (G° of $H_2O_{(g)} = -229 \text{ kJ/mol}$, G° of $Cl_2O_{(g)} = 98 \text{ kJ/mol}$ and G° of $\operatorname{HOCl}_{(g)} = 0 \text{ kJ/mol}$)

| $G^{\circ}_{H_2O} = -229 \text{ kJ/mol}$ $G^{\circ}_{Cl_2O} = 98 \text{ kJ/mol}$ $G^{\circ}_{HOCl} = 0 \text{ kJ/mol}$ | $H_2O_{(g)} + Cl_2O_{(g)} \approx 2 \text{ HOCl}_{(g)}$ $\Delta G^\circ = \Sigma G^\circ_{\text{products}} - \Sigma G^\circ_{\text{reactants}}$ $\Delta G^\circ = [(2 \text{ mol})(0 \text{ kJ/mol})] - [(1 \text{ mol})(-229 \text{ kJ/mol}) + (1 \text{ mol})(98 \text{ kJ/mol})]$ $\Delta G^\circ = 131 \text{ kJ} = 1.31 \times 10^5 \text{ J} (\Delta G^\circ > 0; \text{ Forward Reaction is Non-spontaneous})$ |
|--|--|
| $P_{\rm H_{2}O} = 0.350 \text{ atm}$ $P_{\rm Cl_{2}O} = 0.220 \text{ atm}$ $P_{\rm HOCl} = 0.860 \text{ atm}$ | $Q = \frac{P^2_{\text{HOCl}_2}}{P_{\text{H}_2\text{O}}P_{\text{Cl}_2\text{O}}} = \frac{(0.860)^2}{(0.350)(0.220)} \qquad Q = 9.605194805$ |
| $T = 25^{\circ}C = 298.15 \text{ K}$ $\Delta G^{\circ} = ? Q = ?$ $\Delta G = ?$ | $\Delta G = \Delta G^{\circ} + RT \ln(Q)$ $\Delta G = (1.31 \times 10^5 \text{ J}) + (8.314 \text{ J/K})(298.15 \text{ K}) \ln(9.605194805) = 136608.1798 \text{ J}$ $\Delta G = 137 \text{ kJ}$ |
| | (It became more spontaneous towards the reactants (even more non- spontaneous towards the product side). This probably means that $Q > K$ or $K < 9.605194805$) |

Chemistry AP

Equilibrium Point: - the point where the system attains **thermodynamic equilibrium** – the lowest value of free energy available to the equilibrium system.

- this occurs when $Q = K_P$ and $\Delta G = 0$ at certain partial pressures.
- we can use equilibrium point to calculate the value of the equilibrium constant *K* from ΔG°

Equilibrium Point ($Q = K_P$ and $\Delta G = 0$) of a Gaseous System $aA_{(g)} + bB_{(g)} \Rightarrow cC_{(g)} + dD_{(g)}$ $0 = \Delta G^\circ + RT \ln(K)$ or $\Delta G^\circ = -RT \ln(K)$ $\Delta G^\circ =$ Free Energy (J) of gas at Standard Pressure of 1 atmR = Gas Constant 8.3145 J/K $K_P =$ Equilibrium Constant of Gaseous System $= \left(\frac{P_{C,eq}^c P_{D,eq}^d}{P_{A,eq}^a P_{B,eq}^b} \right)$ T = Temperature in K

<u>Qualitative Relationship between ΔG and K_P : $\Delta G^\circ = -RT \ln(K_P)$ </u>

| $K_P > 1$ | $\ln(K_P) > 0$ (Positive) | $\Delta G^{\circ} < 0$ (Negative) | <u>Products are favoured</u> over the Reactants (Forward Reaction is Spontaneous) |
|-----------|---------------------------|---|---|
| $K_P = 1$ | $\ln(K_P)=0$ | $\Delta G^{\circ} = 0$ | Products and Reactants are <u>Equally favoured</u> |
| $K_P < 1$ | $\ln(K_P) < 0$ (Negative) | $\Delta G^{\circ} > 0 \text{ (Positive)}$ | <u>Reactants are favoured</u> over the Products (Reverse Reaction is Spontaneous) |

Example 3: Calculate the equilibrium constant of the formation of water at 25.0°C. (G° of H_{2 (g)} = 0 kJ/mol, G° of O_{2 (g)} = 0 kJ/mol and G° of H₂O (l) = -237 kJ/mol)

$$2 H_{2(g)} + O_{2(g)} \Rightarrow 2 H_2 O_{(l)}$$

 $\Delta G^{\circ} = \Sigma G^{\circ}_{\text{products}} - \Sigma G^{\circ}_{\text{reactants}}$ $\Delta G^{\circ} = [(2 \text{ mol})(-237 \text{ kJ/mol})] - [(2 \text{ mol})(0 \text{ kJ/mol}) + (1 \text{ mol})(0 \text{ kJ/mol})]$ $\Delta G^{\circ} = -474 \text{ kJ} = -4.74 \times 10^5 \text{ J} \qquad (\Delta G^{\circ} < 0; \text{ Forward Reaction is Spontaneous})$

 $\Delta G^{\circ} = -RT \ln(K_P)$ at thermodynamic equilibrium

 $\ln(K_P) = -\frac{\Delta G^{\circ}}{RT} = \frac{-(-4.74 \times 10^5 \text{ J})}{(8.3145 \text{ J/K})(298.15 \text{ K})} = 191.2085862$ $K_P = e^{191.2085862}$

Since $K_P >> 1$, the equilibrium is <u>extremely favourable towards the product</u> at 25°C. This is in agreement with the conclusion made using the thermodynamic quantity of $\Delta G^{\circ} << 0$.

 $K_P = 1.10 \times 10^{83}$

Example 4: Given that $N_{2(g)} + 3 H_{2(g)} = 2 NH_{3(g)}$ has the following thermodynamic values, calculate ΔG° and K_P of the given equilibrium at 25.0°C.

| Chemicals | H° (kJ /mol) | $S^{\circ} [J/(K \bullet mol)]$ |
|-------------|-----------------------|---------------------------------|
| $N_{2(g)}$ | 0 | 192 |
| $H_{2(g)}$ | 0 | 131 |
| $NH_{3(g)}$ | -46 | 193 |

$$\Delta H^{\circ} = \Sigma H^{\circ}_{\text{products}} - \Sigma H^{\circ}_{\text{reactants}} = [(2 \text{ mol})(-46 \text{ kJ/mol})] = -92 \text{ kJ}$$

$$\Delta S^{\circ} = \sum S^{\circ}_{\text{products}} - \sum S^{\circ}_{\text{reactants}} \Delta S^{\circ} = [(2 \text{ mol})(193 \text{ J/(K} \bullet \text{ mol}))] - [(1 \text{ mol})(192 \text{ J/(K} \bullet \text{ mol})) + (3 \text{ mol})(131 \text{ J/(K} \bullet \text{ mol}))] = -199 \text{ J/K}$$

$$\Delta H^{\circ} = -92 \text{ kJ} = -92000 \text{ J}$$

$$\Delta S^{\circ} = -199 \text{ J/K}$$

$$T = 25.0^{\circ}\text{C} = 298.15 \text{ K}$$

$$\Delta G^{\circ} = 2$$

$$\Delta G^{\circ} = -3.3 \times 10^{4} \text{ J at } 25.0^{\circ}\text{C}$$

$$Since \Delta G^{\circ} < 0, \text{ the Forward Reaction is Spontaneous}$$

$$R = 8.3145 \text{ J/K}$$

$$\Delta G^{\circ} = -32.66815 \text{ kJ} = -32668.15 \text{ J}$$

$$\Delta G^{\circ} = -RT \ln(K_{P}) \text{ at thermodynamic equilibrium}$$

$$\Delta G^{\circ} = -32.66815 \text{ kJ} = -32668.15 \text{ J}$$

$$\ln(K_{P}) = -\frac{\Delta G^{\circ}}{RT} = \frac{-(-32668.15 \text{ J})}{(8.3145 \text{ J/K})(298.15 \text{ K})}$$

$$\ln(K_{P}) = 13.178124$$

$$K_{P} = e^{13.178124} = 528672.2741$$

$$K_{P} = 5.3 \times 10^{5}$$

As we can see $K_P >> 1$, which indicates the equilibrium is <u>favouring the product</u> at 25°C. This is in agreement with the conclusion made using the thermodynamic quantity of $\Delta G^{\circ} < 0$.

Temperature Dependence on K_P:



Example 5: The equilibrium constant of the system, $2 \text{ NO}_{2(g)} \Rightarrow \text{ N}_2\text{O}_{4(g)}$, is allowed to varied with the change in temperature. The experimental data are shown below.

| Temperature | Equilibrium Constant (K _P) |
|-------------|--|
| 373 K | 0.067 |
| 273 K | 58 |
| 195 K | 1.4×10^{6} |
| 77 K | 3.8×10^{29} |

- a. Complete the table below.
- b. Graph $ln(K_P)$ versus 1/T. Determine the slope and *y*-intercept of the graph using linear regression of your graphing calculator.
- c. Calculate the ΔH° and ΔS° of this equilibrium system.
- d. Comment on the thermodynamic spontaneity of the equilibrium system at various temperatures.

| Temperature | Equilibrium Constant (K _P) | $1/T (K^{-1})$ | $\ln(K_P)$ |
|-------------|---|----------------|------------|
| 373 K | 0.067 | | |
| 273 K | 58 | | |
| 195 K | 1.4×10^{6} | | |
| 77 K | 3.8×10^{29} | | |

- a. Using the TI-83 Plus Calculator, we can enter the experimental results in the STATS Editor and quickly manipulate the data.
 - 1. Enter Values in the L₁ and L₂ Columns of Stats Editor

3. Fill in the Table

| Temperature | Equilibrium Constant (K _P) | $1/T (K^{-1})$ | $\ln(K_P)$ |
|-------------|--|----------------|------------|
| 373 K | 0.067 | 0.00268 | -2.703 |
| 273 K | 58 | 0.00366 | 4.0604 |
| 195 K | 1.4×10^{6} | 0.00513 | 14.152 |
| 77 K | 3.8×10^{29} | 0.01299 | 68.110 |

b. Graph $ln(K_P)$ versus 1/T. Determine the slope and y-intercept of the graph using linear regression of your graphing calculator.

We can use the linear regression function of the calculator to find the value of the slope and *y*-intercept for calculating ΔH° and ΔS° respectively.

c. Calculate the ΔH° and ΔS° of this equilibrium system.

$$-\frac{\Delta H^{\circ}}{R} = slope \qquad \Delta H^{\circ} = -(slope)R = -(6869.8282669823 \text{ K})(8.3145 \text{ J/K}) = -57119.18713 \text{ J}$$

$$\frac{\Delta S^{\circ}}{R} = y\text{-intercept} \qquad \Delta S^{\circ} = (y\text{-int})R = (-21.102770455077)(8.3145 \text{ J/K}) = -175.4589849 \text{ J/K}$$

$$\Delta S^{\circ} = -0.18 \text{ kJ/K}$$

For the equilibrium system, $2 \operatorname{NO}_{2(g)} \rightleftharpoons \operatorname{N}_{2}\operatorname{O}_{4(g)}$, it makes sense that $\Delta S^{\circ} < 0$ because it is proceeding from two molecules of gas to one molecule of gas.

d. Comment on the thermodynamic spontaneity of the equilibrium system at various temperatures.

$$2 \operatorname{NO}_{2(g)} \rightleftharpoons \operatorname{N}_{2}\operatorname{O}_{4(g)} + 57 \text{ kJ}$$
 ($\Delta H^{\circ} < 0 \text{ and } \Delta S^{\circ} < 0$) $\Delta G^{\circ} = \Delta H^{\circ} - T \Delta S^{\circ}$

At <u>LOW Temperature</u>, $\Delta G^{\circ} < 0$ (Spontaneous Forward Reaction) because $\Delta H^{\circ} < 0$ and $\Delta S^{\circ} < 0$ (-= (-) - small (-)). This agrees with the fact that $\underline{K_P} >> 1$ at Low Temperature, which indicates that the system favors the product side. (Applying Le Châtelier's Principle will conclude that <u>that at Low Temperature</u>, $[N_2O_4]^{\uparrow}$ and $[NO_2]^{\downarrow}$)

At <u>HIGH Temperature</u>, $\Delta G^{\circ} > 0$ (Spontaneous Reverse Reaction) because $\Delta H^{\circ} < 0$ and $\Delta S^{\circ} < 0$ (-= (-) - big (-)). This agrees with the fact that $\underline{K_P < 1}$ at <u>High Temperature</u>, which indicates that the <u>system favors the reactant side</u>. (Applying *Le Châtelier's Principle* will conclude <u>that at</u> <u>High Temperature</u>, $[N_2O_4] \downarrow$ and $[NO_2] \uparrow$)

> <u>Assignment</u> 18.6 pg. 811–814 #21, 22, 24, 26 to 32, 49, 64, 66, 76, 80

Copyrighted by Gabriel Tang B.Ed., B.Sc.

Page 295.